NOISE MEASUREMENTS DURING APPROACH OPERATIONS ON RUNWAY 21R AT DETROIT METROPOLITAN AIRPORT

Dwight E. Bishop

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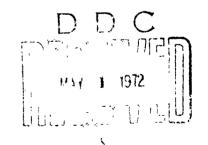




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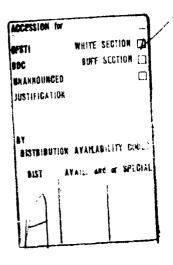
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Systems Research and Development Service

Washington, D.C. 20591

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LIST OF ABBRTVIATIONS AND SYMBOLS

AGL above ground level

D duration correction in dB

d duration time, sec.

EPNL effective perceived noise level in EPNdB

IFR instrument flight rules

ILS instrument landing system

IP glide slope intercept point

MSL above mean sea level

NEF noise exposure forecast

OM outer marker

PNLC composite perceived noise level in PNdB

PNLM maximum perceived noise level in PNdB

PNLTM maximum tone-corrected perceived noise level in PNdB

SENEL single event noise exposure level in dB

TRACON terminal radar approach control

1. INTRODUCTION

This report presents noise and other data acquired during two 10-day periods of aircraft noise measurements at three locations under the ILS (instrument landing system) approach path to runway 2JR at Detroit Metropolitan Airport. The field measurements were made in May and June of 1971, preceding and during Phase A of a planned three phase "field evaluation of the 3,000 ft glide slope intercept program" jointly conducted by the FAA Aircraft Traffic Service, Office of Aviation Policy and Plans, and the Division of Noise Atatement, Systems Research and Development Service. The noise measurements, together with weather and distance information, were acquired by Bolt Beranek and Newman Inc. (BBN) as authorized under FAA Contract DOT-FA71WA-2589. The noise measurements form one part of FAA studies of air traffic procedures which might reduce aircraft noise exposure near alreports.

Ine aircraft noise and distance data provide basic information for evaluating changes in the noise environment under and in the vicinity of approach paths to runway 21R during IFR (instrument flight rules) operations under differing air traffic procedures. During the two measurement periods, noise of individual aircraft approaches was recorded; the recorded noise signals were later reduced to obtain effective perceived noise level (EPNL) values and other noise measures. Whenever possible, photographs of the aircraft were taken at each measurement posstion to establish aircraft identification and to determine the "distance of closest approach" to the

^{*} References are listed together at the end of the report.

measurement position. From the EPNL data and number of observed approaches, noise exposure forecast (NEF) values describing the noise environment resulting from IFR operations were calculated.

The test program (particularly as it pertains to the planning of the noise measurements) and the data acquisition and data reduction procedures are reviewed in Section II of the report. Noise, distance and weather data are given in Section III. NEF values and mean EPNL values are reported in Section IV. The final section of the report, Section V, compares the mean EPNI and NEF values observed for the two test phases.

This report is limited to presentation of basic noise and distance data, and calculation of NEF and mean EPNL values at the measurement positions. Further analysis of the aircraft noise and distance data will be reported separately.

II. TEST PROGRAM OUTLINE AND TEST CONSTRAINTS

A. Runway 21R Approach Path

As noted in the introduction, the major purpose of the noise measurements was to provide basic information for evaluating changes in the noise environment in land areas near IFR approach paths under differing IFR traffic procedures. IFR approaches utilizing ILS facilities at Detroit Metropolitan Airport (DTW) may occur on any of three runways -- 21R, 3L and 27 - with radar approach control services provided by the terminal radar approach control (TRACON) room located at the airport terminal.

Approaches on runway 21R were selected for the noise measurement as this runway is one of the two most frequently used instrument runways. Land under the approach paths to runway 21R is also more highly developed and urbanized than the areas under the other IFR approach paths. At DTW, approaches frequently shift from one runway to another due to changing wind conditions, introducing variability in the number of approaches observed per day on any of the runways.

The major instrument approach paths to runway 21R, as defined by the local F4A air traffic staff, are sketched in Fig. 1. Also identified in the figure is the location of the outer marker (OM) and the intercept points (IP), the points at which the aircraft should ideally intercept the 2.8° glide slope altitude profile. Under ideal conditions, the aircraft should intercept the localizer at the "turn-on" point, which is three nautical (n) miles from the IP.

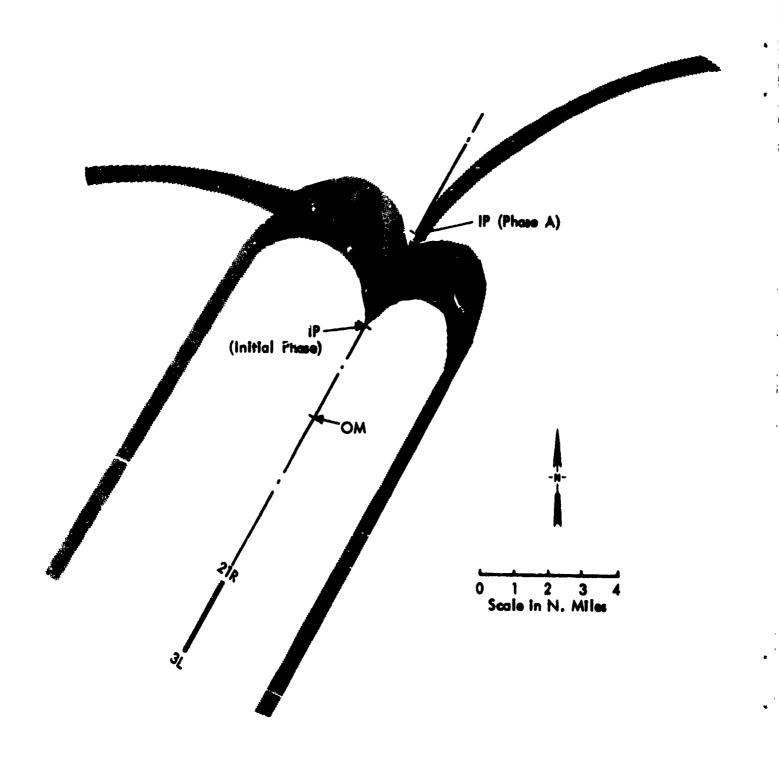


FIGURE 1. TYPICAL APPROACH PATHS FOR ILS LANDINGS ON RUNWAY 21L - CURRENT OPERATIONS (INITIAL TEST PHASE)

One will note from Fig. 1 that aircraft approach the ILS landing track from several directions. Also to be noted is that the point at which the aircraft turn on to the localizer is variable. It is heavily dependent upon the volume of traffic and number of aircraft being handled. As approach traffic increases in volume, the point at which the aircraft intercept the localizer track moves further from the runway.

B. Test Program Description

The first set of noise measurements, taken between 17 and 26 May, was conducted using current (non-test) IFR procedures at the airport. (These are identified as "initial phase" measurements throughout the report.) The second series of measurements, between 2 and 11 June, was conducted during the Phase A test procedures.

During each series of measurements, noise from aircraft ILS approaches was measured between 0600 and 2400 hours at each of these measurement positions.

The typical altitude profile for current (non-test) ILS approaches on runway 21R is shown in Fig. 2, identified as the "initial phase" profile. Under this procedure, aircraft remain in level flight at 3,000 ft above mean sea level (MSL) (approximately 2,400 ft above ground level (AGL))until intercepting the 2.8 degree glide slope. Under ideal conditions the turn-on point (the point at which the aircraft should intercept the localizer) is approximately 10.9 n miles from the runway threshold (or 5.7 n miles from the OM which is located approximately 5.2 n miles from the runway threshold). The aircraft would intercept the glide slope (on course and at proper altitude) at the IP, approximately 2.7 n miles from the OM.

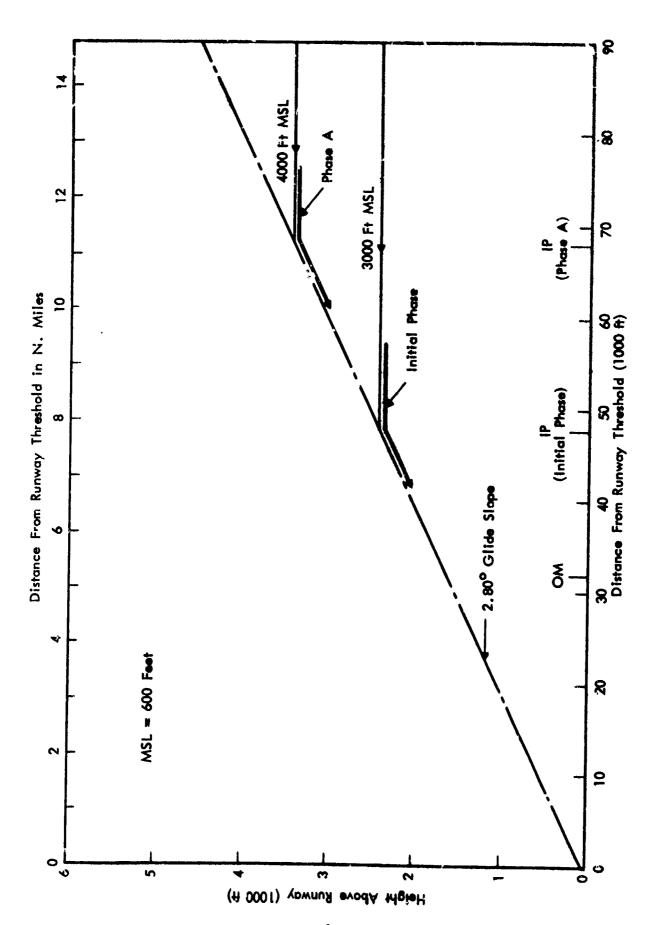


FIGURE 2. IDEALIZED AIRCRAFT DESCENT PROFILES

For the Phase A tests, the aircraft altitude prior to interception of the glide slope was increased to 4,000 ft MSL (approximately 3,400 ft AGL). This Phase A profile is also shown in Fig. 2. When the intercept altitude is increased to 4,000 ft MSL, the IP moves out to 11.3 n miles from the runway threshold, and the turn-on point is shifted to 14.3 n miles from threshold.

The increase in intercept altitudes from 3,000 to 4,000 ft should result in lower noise levels under the approach path at positions beyond the initial thase IP. For example, the EPNL vs slant distance curves for four-engine turbofan aircraft on approach, often used in NEF computations, indicate a decrease of EPNL of approximately 10 EPNdB per doubling of distance for slant distances in the range of 1,000 to 4,000 ft.2 On this basis, one would estimate a reduction of about 5 EPNdB in typical noise levels for the increase in intercept altitudes.

C. Selection of Measurement Positions

While verification of a difference in noise levels with altitude ur r controlled tests of a given aircraft would be relatively straight forward, field verification of such moderate changes in noise levels between test phases is, in practice, quite difficult for several reasons:

- a. Variability among aircraft and in aircraft operating conditions (i.e., engine and flap settings, airspeed, etc.);
- b. Variability in weather conditions;
- c. Dispersion in flight tracks prior to interception of the glice slope;
- d. Differences in flight tracks (prior to interception of the glide slope) between test phases.

A further factor acting to reduce the number of IFR approach flights which can be used to compare differences in test procedures is the fact that it is quite common, under good weather and light traffic conditions, for commercial aircraft operating under IFR to make a visual approach to the airport. Such aircraft, particularly when approaching Detroit from the south, may well turn on final arproach near or inside of the outer marker and hence would not pass over measurement stations located under the normal IFR flight path.

As a consequence, the following rationale was adopted in establishing noise measurement positions. One position (Station A), was maintained at the OM during octh measurement phases. Data from this position help identify differences in test data on a day-to-day basis occurring because of weather and shifts in runway usage. Data from this position also serves as a basis for "normalizing" NEF values to account for the varying numbers of operations observed on the different test days.

The remaining two measurement positions were located between the IP and the turn-on point. Positions further out on the approach path were not selected because of the dispersion in flight tracks.

Selection of actual field positions was further modified by the particular needs for:

- a. An open space for visual observation of the flights;
- b. Low ambient noise levels, which meant avoidance of positions close to local traffic or heavy highway traffic.

Since the approach paths, particularly beyond the outer marker, are over dense urban areas, the above considerations drastically limited the choice of sites.

Table I identifies the measurement stations. Their location with respect to the approach path profiles is shown in Fig. 3. Figure 4 shows the location of the stations with relation to the ILS flight track.

While measurements were made only at three positions simultaneously, a total of four different positions were employed during the Phase A measurements. Stations A and D were used throughout. However, measurements were shifted from Station E to Station F after several days of measurement because of the high ambient noise levels and wide aircraft path dispersion encountered at Station E.

D. Noise Data Acquisition and Reduction Procedures

Each measurement station had self-contained recording capability, utilizing the following instrumentation components:

Bruel & Kjaer Type 4133 1/2-in condenser microphone Electro-Voice 355 Windscreen

Bruel & Kjaer Type 2619 preamplifier (or Hewlett-Packard Type 15018B preamplifier)

Bruel & Kjaer Type 2203 sound level meter

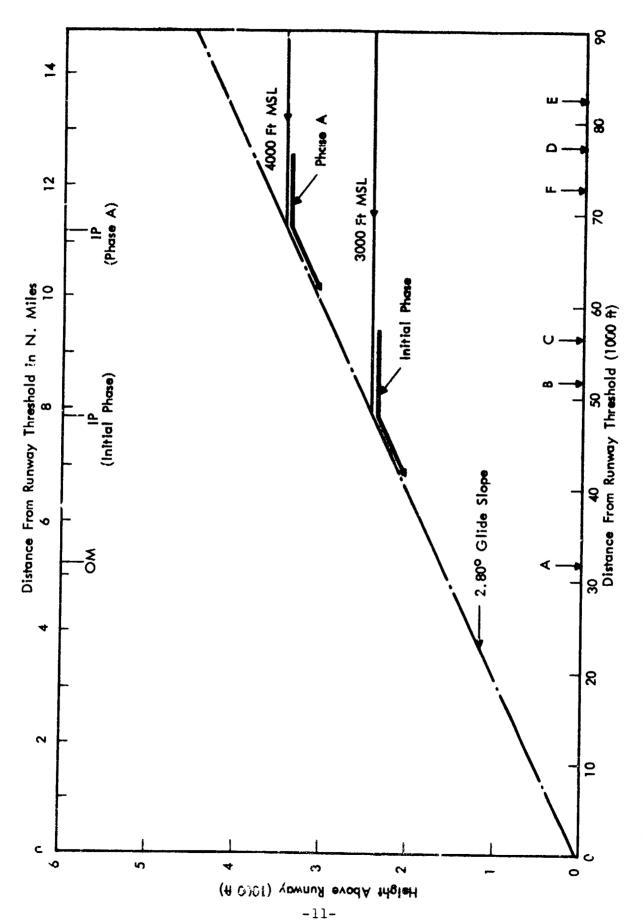
Kudelski Nagra III Tape Recorder

Bruel & Kjaer Type 4220 Pistonphone Calibrator

For meteorological data, each station was equipped with a psychrometer and an anemometer. Each station also had a 35 mm camera with appropriate lenses to photograph the aircraft. A VHF receiver enabled the operator to keep informed of the current air traffic situation.

TABLE I
LOCATION OF NOISE MEASUREMENT STATIONS

Test Phase	Measurement Station	Location
Initial and A	A	400' N of Avondrle on the service road to Westwood Park in the City of Inkster. (This site is in the immediate vicinity of the outer marker for ILS Runway 21R.)
Initial	В	In River Rouge Park, 150' W of Outer Drive, 1000' S of Joy Road.
Initial	С	In River Rouge Park, near the nursery.
А	D	In the nursery just west of the inter- section of Oakfield and Santa Maria.
A	E	On Forrer near the intersection with Clarita.
А	F	NW of the intersection of Bretton and Glastonbury in North Rosedale Park.



LOCATION OF MEASUREMENT POSITIONS WITH RESPECT TO FIGURE 3.

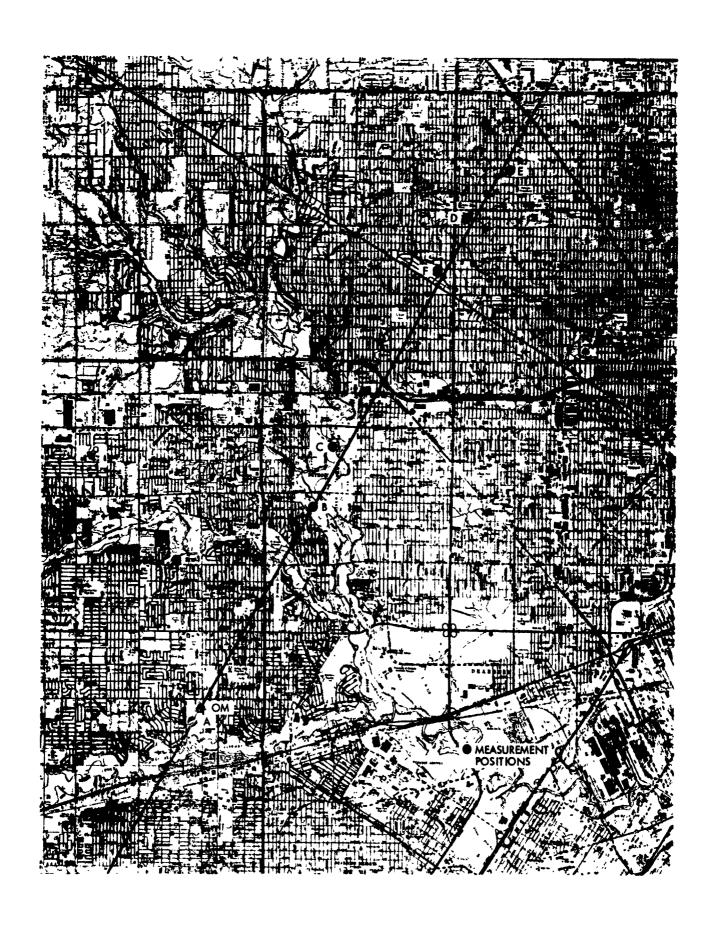


FIGURE 4. LOCATION OF MEASUREMENT POSITIONS WITH RESPECT TO RUNWAY 21R ILS FLIGHT TRACK

Field measurements consisted of recording on magnetic tape the ambient and flyover noise levels for each event. In addition, whenever possible, a photograph of the aircraft was obtained. The photographs were taken at the time when the aircraft was judged to be closest to the observer.

Once each hour, or more frequently if weather conditions made this desirable, a relative humidity measurement was made and an average wind speed reading taken.

Pistonphone calibration signals were recorded at the beginning and end of each reel of tape. If runway 21R was not used for any length of time a new calibration was performed when the runway was reactivated. Additionally, one set of insert resistor calibration gear was available and insertion calibrations were performed by supervisory personnel.

The magnetic tapes recorded in the field were analyzed in the laboratory using a Hewlett-Packard 8054-A Real Time Audio Spectrum Analyzer under the control of a Digital Equipment Corporation PDP-8 computer. The computer causes the recorded signal to be sampled at 1/2-second intervals, makes corrections for background noise levels, and corrects the whole system to flat response. (In this context the system is viewed as all equipment from the microphone to the input of the spectrum analyzer and corrections therefore include microphone sensitivity, record-playback characteristics of the tape recorders and all calibration data as recorded in the field.) The digitized noise data are then used to calculate the various noise levels.

More detailed descriptions of the data acquisition and data reduction instrumentation and of data handling procedures are given in Appendix A.

III. DATA PRESENTATION

A. Number of Flights and Field Measurements

Table II shows the total number of noise recordings made per day during the hours from 0600 to 2400 during the field measurements. The table also lists the number of field recordings which were later reduced to obtain aircraft noise levels. A total of 4059 field recordings were obtained, with over 1400 recordings reduced to obtain noise level data.

For comparison, Table III and Fig. 5 show the expected total number of arrivals of scheduled commercial aircraft at Detroit Metropolitan Airport, based on an analysis of the airline schedules for May 1971 published in the Airline Guide. 3/ Figure 5 also shows the total number of scheduled turbojet and turbofan aircraft (excluding propeller aircraft). The total number of scheduled airline arrivals was 278 per day with over 97 per cent of the arrivals occurring between 0700 to 2400 hours. Although a number of IFR landings of non-scheduled aircraft occur, the scheduled transport aircraft can be expected to account for a very large proportion of the IFR arrivals at Detroit Metropolitan Airport.

Part of the first day for each measurement period (May 17 and June 2) was devoted to instrumentation checkout and crew training, hence noise measurements for these days are incomplete. However, for the remaining days in each period, the number of field recordings noted in Table II corresponds essentially to the number of aircraft on approach passing near the respective measurement positions between the hours of 0600 to 2400. Aircraft well off to the side of the measurement stations were not recorded, since such aircraft were not judged to be on IFR approaches.

TABLE II
TOTAL STREET OF NOISE IGAS-TREMSTA

The second of th

A - IMPRIAL PRACE HEADWHINES

		P1014	Naise Room Pagitians	relings		Rede	red Noise D	hte	
Date	Period	^	3	C	Total No.	A	•	С	Total
5-17	D E	4.5	21	17	10/5				
5-18	D E N	125 35 6	61 72 2	60 20 2	2AF 77 10	97 34 6	38 10 . 2	45 17 2	180 69 10
5-19	D E N	84 7 12	72 3 2	61 1 2	21? 11 16	31 6 6	22	24	77 6 6
5-20	D E N	138 2 3	73 1 2	73 1 1	284	22	18	23	63
5-23	D E N	85 29 6	39 12 3	28 15 2	157 76 11	2)	10 7 2	6 11 2	39 26 7
5-24	D E N	95 7	59	71 3	225. 14	19	18	20	57
5- 25	D E N	182 29 7	92 22 1	125 16 7	399 65 15	50 53	17 12	17 7 2	57 39 2
5-26	D E N	45 10 13	27 12	20 7 1)2 23 18				

D. PHASE A MEASUREMENTS

		P1	eld Moise	Recerdin	Ç8			Reduced N	oise Data		
			Posi	tions.			<u> </u>	Pos1	tions		
Date	Period	A	D	ı	7	Total No.	A	D	E	7	Total
6-2	D E N	69	21	42		138	24	5	7		36
6-3	D E N	159 42 12	78 18 3	87 15		324 73 19	21 20 3	19 5 2	13 4 1		53 29 6
6-4	D E N	99 10	51 3 1	55 1		205 13 6	20 3	16 2	11		47 2 3
6-5	D E N	46 23 10	28 7 2		40 6 1	114 36 13	21 18 2	11 3		12 4 1	41 25 3
6-6	D E N	69 36 13	41 25 5		30 11 2	140 73 20	20 18 2	12 11		12	44 31 2
6-7	D E N	158 *1 11	99 19 ?		137 29	394 89 13	146 24 9	68 5 2		83 12 1	298 41 12
6-8	D E M	35	12		18	65	19	5		3	27
6-10	D E N	30 3	10		9	40	21	5 1		3	29 2
6-11	D R	72 40	24 21		43 22	139 83	16 13	8 12		2 12	26 37

TABLE III

TOTAL NUMBER OF ARRIVALS OF SCHEDULED COMMERCIAL AIRCRAFT
AT DETROIT METROPOLITAN AIRPORT, MAY 1971

Hour	Number of Arrivals
Midnight to 0059	4
0100 to 0159	1
0200	0
0300	1
0400	0
0500	2
0600	4
0700	11
0800	20
0900	16
1000	18
1300	16
1200	13
1300	9
) #00	16
1500	24
160)	21
1700	14
1800	23
1900	27
2000	14
2100	14
2200	7
2300	3

^{*} Based on May 1971 issue of Official Airline Guide, Quick Reference, North American Edition.

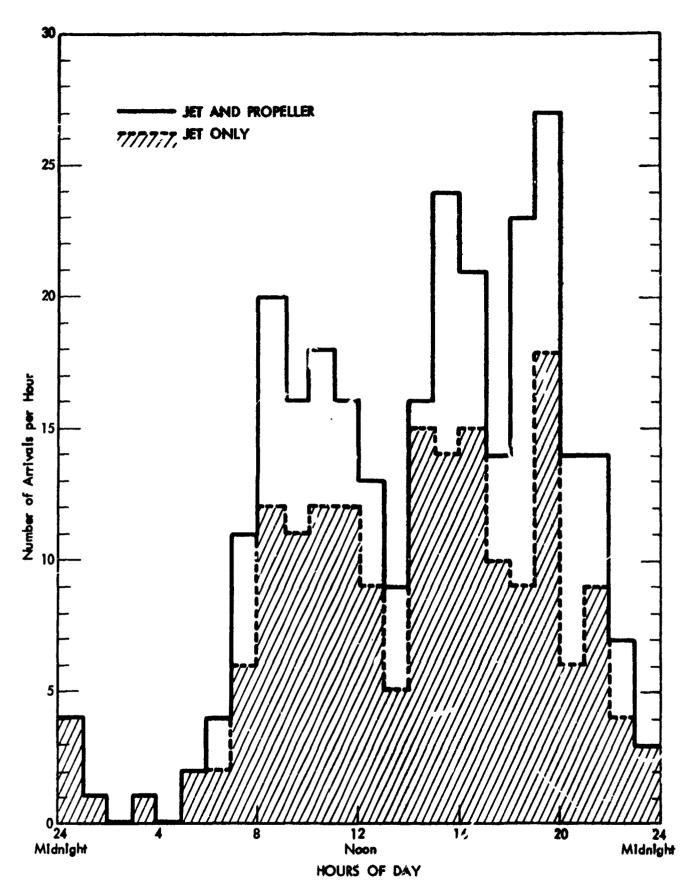


FIGURE 5. SCHEDULED AIRLINE ARRIVALS AT DTW (MAY 1971)

The variation in the number of field recordings per day listed in Table II reflects the large variability in runway 21R utilization, with operations shifted to other runways quite frequently. Also to be noted from Table II is the fact that more aircraft were observed at position A than at the outer positions.

For one day of each test period (May 18 and June 7), all useable recorded data were analyzed. For the other test days, samples of recorded noise data were reduced. In selecting the recordings to be sampled, propeller aircraft recordings were omitted. These aircraft were significantly less noisy than the jet aircraft, hence contributed little to the NEF values. Jet aircraft recordings were selected to obtain an approximate balance between four-engine, and two- and three-engine jet aircraft. Further selection was made to obtain a distribution of recordings during morning, afternoon, evening and night periods.

B. Weather Information

Weather information during the hours of field measurement is summarized in Table IV. This table lists the temperature, relative humidity, barometric pressure, and wind direction and speed reported by ESSA at Detroit Metropolitan Airport, and the temperature, relative humidity and wind speed observed at the individual measurement positions. Data are listed at hourly intervals spanning the period of field measurements.

C. Noise and Distance Information

Table V presents the noise and distance information obtained during the field measurements. Data are listed in the table according to position, date and time of recording. Aircraft identification was established by inspection of photographs

TABLE IV MEASURE PROMEY

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Date	Time Est	138	M Wea	ther Bur	wau, Ai	rport]	1	1014			,	1014		ļ	,	1014	
	:	ī,	Rel. Hum.	Po 1n.	Vind Dir.	V1 ted Speed	706	Ţ	Rel. Hum.	Wind	700	1	Rei.	Vint	700	: ••	Rel.	Wind
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	15 16	76 76	31 30	29.200 29.180	160 160	12 12	A	73 75	42 37 42	0f 09 0 8		77	67	08	C	77	61	05
	17 18	75	33 35	29.170 29.165	170 170	11 10	1 1	72 69	42 51	0 8 04		75	39	05	C			•
May 18	6	56	86	29.140	160	07	,	58	97	02		65	70	07		62	70	0.2
, may 20	7	64	73	29.150	190	10	A	63	87	09	B	70	68	Ċ9	C	69	79 67	03 08
	8 9	70	63 52	29.150 29.140	200 230	12 15	A	71 76	72 59	10 10	B	73 79	61 55	0 6 12	e e	75 79	58 53	10 12
	10	77	49	29.140	230	15	A	76	59	08		85	50	18	C	82	5í	10
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	15 16	88 87	29 30	29.100 29.110	220 240	19 17	1 1	87 88	38 39	17 08	B	89 88	33 34	26 16	C	86	37	10
	17	84	35	29.095	230	14	l â	00	37	00	B	86	33	09	Ìċ	85	37	32
	18	B4	35	29.095	230	15	A	82	47	06	В	85	33 36	09	C		-	
	19 20	81 73	41 46	29.090 29.085	220 180	10 07	A	78 73	54 57	05 C0	. B	80	45	05	C	79	46	07
	21	73	53	29.100	190	09	l î	71	68	00	B				0000			
	22	72	55	20.100	190	08	A	70	72	00	В	75	54	05	Ċ			
	23 24	70 69	61 66	29.100 29.100	170 130	07 07	1 1	67 66	80 85	00 00	B	72	Éì	05	C			
May 19	6	52	81	29.115	180	08	1 2	62	94	09	B	67	78	30	c	v5	80	04
,	7	67	70	29.120	180	11	Ä	64	90	09	В	70	72	07	C	69	70	04
	8	71	64	29.115	200	12		71	79	10	В	74	65	10	С	75	65	05
	10	75 78	56 50	29.115 29.095	210 220	16 16	1 1	72 75	69 66	10 12	B	77 79	59 55	16 14	C	77 78	57 54	07 04
	11	79	49	29.095	220	17	Ä	79	57	10	В	83	49	26	č	81	48	0ê
	12	82	44	29.070	500	17	1 1				В	84	43	18	Ç	81	48	04
	13 14	83	41 40	29.070 29.050	190 210	20 18	1 1	84	44	07	B	84 84	46 46	30 08	ç	83 84	49 4£	15 12
	15	83	41	29.045	200	50	Ä	83	49	10	8	84	46	22	C	-	70	12
	16	81	46	29.025	200	16	!	81	55	08	В				Ç	81	55	12
	17 18	65	90 84	29.050 29.100	260 270	07 14	1 1				B				ç			
	19	64	84	29.130	210	06	l â				B				lč			
	20	63	87	29.150	1F0	06	A				3				C			
	21 22	62	90 70	20.180	240 290	04 12	1 4	64	70	09	B	61	68	09	C	61	63	04
	23	57	72	29.250	310	10	l ä	04	,,,	0,	1 5	57	66	12	č	58	63 66	08
	24	54	69	27.280	320	10	Ä				В	•			Ċ	53	75	00
May 20	6	45 47	93	29.305	220	05	A	49	93	00	В	51	84	00	Ç	50	93	
	7 8	51	93 86	20.320	230 230	0? 05	^	51 57	81 65	00 02	B	56 61	82 73	04 10	C	59	78	06
	9	60	70	29.325	180	11	Â	57 63	62	06	В	65	59	12	C	65	56	10
	10	64	50	29.320	200	13) A	65 66	54	10	B			18	C	69	55	12
	11 12	65 66	50 49	29.310 29.300	240 220	10 14	A	66 68	55 56	10 04	B	68 67	50 51	12 08	e c	66 66	53 53	12 08
Ī		, "	٠,	-,.,00		• •	I ^	~	,,,	-	1 "	٥,	,,	-	1 "	50	23	

TABLE TV (Con't)

Date	Time EST	ESSA Weather Bureau, Airport T Rel. P. Wind Wind			rport		,	1+16			,	ield		P101 1				
		î °p	Rel. Hum.	P 1ñ. Hg.	Wind Dir. • Nag.	3p4ad	Pos	ī,	Rel. Huti.	Wind Speed ka	Pre	Ĩ,	Nol. Num.	Wind Speed kn	Pos	Ŧ,	R(1. Ht. 1.	Wind Speed kn
May 20	13 14 15 16 17 18 19	63 64 68 69 66 66 65	73 47 41 37 34 39	29.295 29.295 29.285 29.235 29.290 29.300 29.320 29.340	250 250 260 290 290 290 320 310	1 ³ 07 13 15 15 12 12	A A A A A A	69 69 68 71 65 65 65	97 97 97 86 44 37	67 10 08 10 05	8 8 8 8 8 8	65 67 69 71 69 63 54	59 49 49 41 3:1 53 36	05 10 12 12 08 09 07	0000000	64 69 69 68 67	58 47 43 38 37 36	09 12 10 10
May 23	9 10 12 13 14 15	60 62 63 64 65 67 68	58 46 41 40 40 37 37	29.405 29.395 29.385 29.375 29.335 29.330 29.300	120 150 130 150 140 140	13 12 13 15 07 06 08	A A A A A A A	65 67 69 7 67 7 67	46 45 45 45 49 49	10 10 10 02 96 04	8 8 8 8 8 8	66 68 68 71 71 68	53 42 46 54 40 39	08 12 16 10 10 14	0000000	63 65 66	15 44 40	37 08 07
	17 18 19 20 21 22 23	68 66 63 51 57 53 53	3561 41 45559	29.265 29.230 29.215 29.210 29.210 29.210 29.210	130 140 140 120 120 110 110	09 10 07 10 10 98	A A A A A	73 74 64 67	46 43 47 48	02 07 10 10	8 8 8 8	70 67 63 60 59	38 41 50 48 47 47	10 10 08 14 10	00000000	72 65 59 59	38 39 4#	03 05 04 05
May 24	12 13 14 .5 16 17 18 19 20	. 65 68 74 76 75 74 70 66 62	84 769 642 64 570 87	28.975 28.980 28.955 28.945 28.995 28.990 28.910 28.940 28.930 26.910	180 200 220 230 210 190 190 220 240 190	14 13 12 13 12 12 15 18 09	A A A A A A	68 72 77 75 76 76 72	76 75 67 66 64 55 57	09 07 07 07 10 11 08	8 8 8 8 8 8 8	72 75 77 77 71	91 66 67 61 58	12 18 14 09 20	000000000	67 76 75 80 75 73	80 66 70 91 66 53	04 04 10 06 06 07
May 25	7 8 9 10 11 12 13 14 15 16	58 58 58 56 56 56 56 55 55	90 81 78 69 62 72 77 69 72 72 68	28.920 28.835 28.835 28.885 28.905 28.915 28.945 28.965 28.965 28.965	230 230 240 250 250 250 220 250 240 260 250	19 13 15 16 13 15 14 16 17 15 20	A A A A A A A A A A	59 660 57 58 55 55 55	78 68 63 68 71 69 69 64 71	11 10 21 12 14 12 08 08	8 8502 5 L88888	61 62 60 60 60 57 57 57	94 66 68 68 73 71 71 74	26 18 20 16 24 22 20 22 22	0 0000000000000000000000000000000000000	60 60 60 58 60 59 58 55 55	78 78 63 72 68 67 67 66 76	0E 12 10 10 10 16 14 14

TABLE IV (Con't)

Dete	Time Ber	ESS	A Wes	ther Dur	eau, Ai	rport		1	1-14			,	1016			,	1+16	
		T.	Rel. Hum. %	in. Mg.	Vind Dir. • Not.	Vind Speed kn	Pos	7	Rel. Hum. g	Vind Reads (t)	764	Ţ	Rel. Num.	Wind Speed kn	Pos	ī,	Rel. Num. S	Vind Speed kn
Pay 25	18 19 20 21 22 23 24	54 53 52 50 49 49	66 69 74 83 89 86 86	29.015 29.035 29.035 29.075 29.085 29.085	240 240 250 250 250 250 240	20 16 17 15 14 13	A A A A A	54 52	70 \$1	10	3 3 3 3 3	55 55 54	70 70 76	09 06 06	0000000	54 55 51 51	70 75 81 75	15 98 98 98
May 26	6 7 8 9 10	48 48 46 49 49 51	86 83 80 74 74	29.140 29.176 29.161 29.163 29.268 29.220	250 269 270 260 270 270	14 14 11 12 15	12444	51 51 52 54	75 83 72 69 67	06 06 07 06 09 C4	B B B	50 50 51 52 52 51	80 77 75 72 71 71	12 14 16 12 14	000000	49 51 52 51	80 39 75 75	08 12 11 12
	20 21 22 23	50 49 49 48	68 71 71 74	29.350 29.350 29.350 29.300	250 240 260 290	10 08 12 12	A	51 51 49	84 72 73	0 6 07 02	8 8 8 8	51 51 50	71 75 74	08 08 03	CCCC	51 49	75 80	02 05

TABLE IV (Con't)

Jete	Time EST	Z33	A Wea	ther Bur	esu, A	rport		,	ield			,	1014				1014	
		T _p	Hei.	Po in. Ng.	Vind Dir. • Nag.	Vind Speed kn	Pos	Ţ.,	Rel. Hum.	Vind Speed in	Pos	; •	Rel. Nam.	Vind Speed kn	Pos	:,	Rel. Nam.	Wind Speed ice
Jame 2	14 15 16 17 18	71 74 75 77 77	76 66 64 62 50	29.270 29.230 29.220 29.195 29.210	230 230 230 250 270	12 14 16 17 19	A A A A A	78 78 78 75	67 63 49 56	08 07 12 10	D D D	78 76 74	63 64 61	04 10 05	E E E	78 76	6 0 6 2	10 12
June 3	19 6	71 51	57 96	29.260 29.415	300 240	18 04	A	70	59	09 06	D				E	70	55	10
	7 8 9	56 62 66	93 84	29.435	240 230	07 08	^	61 65	84 77	06 07	D	5 8 61	88 84	03 03-10	E	57	94	00 05
	10 11 12 13	69 10 72 75	73 66 64 63 56	29.455 29.455 39.465 29.460 29.445	250 280 280 280 280 280	09 11 12 12	444	70 71 75 75 77	70 68 64 56 59	07 09 08 08 05	0000	65 69 72 75 77	80 76 69 58	96 03 06 10	EEEE	67 70 74	71 68 58	05 05 05
	14 15 16 17	77 78 80 50	55 50 49 51	29.435 29.625 29.415 29.420	280 280 290 260	10 11 9 10	A	77 80 81 82	61 54 51 49	05 06 06 08	0000	78 81 83	52 53 51 52 49	03 08 05 05 04	E E E E	78 80 81 80	53 54 48 50	05 08 05 05
	18 19 20	80 77 71	49 56 67	29.410 29.400 29.400	250 240 220	09 08 05	A	79 74	45 47	07 00	D D	82 76	55 62	06 00	E	81	48	00
	21 23 24	68 69 65 62	73 71 78 90	29.405 29.415 29.420 29.425	210 210 220 280	05 05 03 06	AAA	€9 66 65	79 37 85	00 00 00	0000	70 68 67	72 80 75	00 00 00	E E E E	75 72 68 67	62 69 76 80	00 00 00 00
Jui. 4	િ 7 ફ	58 64 69	93 84 71	29.465 29.465 29.485	200 250 300	03 03 02	A	62 61 72	89 75 69	00 04 06	D D	65 70 74	75 64 58	00	E	65 70	75 64	00 00
	15 -1	75 79 80	59 49 53	29.480 29.475 29.475	250 070 280	04 02 07	Ä	во	57	04	D D	81 82	51 55 47	06 00	E	74 77 81	58 56 58	00 06 03
	12	81 83 84	46 46	29.485 29.445 29.425	200 240 280	07 06	Å	85 85	48 50	06 05	D D	85 86 88	50 43	04 02 04	meim	82 85 88	51 47 46	00 02 04
	16 17	84 84	45	29.420	250 250	06 07 10	A A	87 87 87	43 43	07 05 05	000	88 88 88	46 35 40	04 04 05	E E	85 88	44	03 07 00
	18 19 20	82 84 81 80	53 48 51 51	29.400 29.390 29.390 29.385	230 250 290 290	06 06 05 04	A	86 84	48 49	00 03	D D D	85 84 80	53 49 61	00 00 05	EEE	86	47	0,
June 5	6 7 8 9	64 67 73	86 84 71 65	29.390 29.390 29.385 29.370	280 290 050 150	03 04 04 05	A A A	64 68 73 78	97 90 86 75	00 00 00 04	D D D	68 73 78 80	80 69 67 61	00 00 00	P P	67	85	00
	10 11 12	80 82 80	60 58 67	29.280 29.360 29.350	210 180 160	06 08 10	A	80 78	75	03	D D	80 83	61 58	00 03	F P	80	72	05
	13 14 15 16	82 83 84 82	59 61 59 63	29.350 29.340 29.310 29.290 29.260	160 130 110 140	09 09 08 11	A A A	78 81 77	75 77 70 79	04 09 05 00	00000	84 85 84 81	59 53 59 61	06 03 03 06	P P P	85 83 85 83	ό0 52 60 6 2	05 06 05 04
	17 18 19	74 73 70	82 84 84	29.265 29.245 29.245	080 120 120	08 13 08	Â	72 70	98 98	08 10	D D	75 73 71	86 86 81	02 04	P P	73 69	86 90	00 00
	20 21 22	66 64 64	81 90	29.270 29.260	160 130	10 06	Ā	63 64	97 90	94	D D	67 65	75 80	00 00	P P P	64	92	00
	23	63 62	90 90 90	29.240 29.250 29.245	310 130 120	04 06 06	A	63 62	89 97	00	D D	65 65	80 80	00	P	63	89	00

TABLE IV (Com't)

Date	Time EST	ESS	ESSA Weather Bureau, Airport					Fie ld				,	1014			Pield			
		7 •p	Rel. Mum.	Po in. Mg.	Wind Dir.	Vind Speed in	Pos	Ţ,	Rel. Num.	Wind Spood kn	Pos	; •	Rel. Num.	Wind Speed kn	Pos	Ť,	Rol. Hum.	Vind Speed kn	
June 6	6 7	66 68	94	29.220	240 260	06 06	A	70 72	90 86	00 05	D	6 8 72	90 82	0 0	!	67	90	00	
		738028775900742	9347 7486 7676 7666 7696 89	29.230 29.230 29.240 29.330 29.250 29.250 29.270 29.170 29.170 29.170 29.160	250 250 220 240 300 060 060 210 210 200 210 210 210 210	06 06 09 17 08 06 06 06 06 07	A A A A A A A A A A A A A A A A A A A	76 81 88 83 84 82 79 75	78 69 63 65 51 66 76 82	06 00 04 07 07 09 04 08 05	00000000000000	80 82 83 82 68 72 79 83 80 77	72 65 65 69 90 82 68 55 51 64 71	02 03 03 00 00 00 00 00 00 00	*****	78 79 82 76 75	75 71 58	00 00 00	
	21 22 23 24	71 72 72 71	87 62 72 71	29.160 29.160 29.160 29.130	230 230	10 11 19 03	Â	74 75 74 70	83 76 89 86	02 07 04 00	0000	76 74 74	74 82 78	05 05 05	F F	73	9€	02	
June 7	57 20 11 12 13	667 702 78 90 83 84	76 75 76 70 67 67 67 58	29.175 29.175 29.160 29.150 29.150 29.150 29.150 29.150 29.150	210 220 210 230 230 230 230 220 210	10 07 08 29 10 12 14 15		7004 7007 888 887 888 888 888 888 888	77496063276	06 07 12 08 10 12 15 12 08	400000000	75 71 7* 77 82 86 87 88	68 72 74 71 65 63 66	002 003 005 005 005 005	F	75 73 75 79 85	74 73 66 71 76 66	C3 C5 C5 C5 C5 C4	
	14 15 16	81 70	57 76	29.015 29.055	230	15 14	Ä	85 72	57	07 00	0 0	85		Šŧ	F	85	57	58	
	. ê	71	82 76	29.050	220 200	04 06	1 4	73 78	82 71	00 03	0	75	86	2	F	71	36	50	
	19 . 3, . 1	69	66 7£	29.061	210 180	09 08 07	Å	74 73	69	03 07	000	73 69	82 95	52 52	F	7€	7C	95	
	23	69	79 84 84	29.06 29.060 29.060		08 06	^	72	86	00	0 0	69 69 69	95 95 95	05 05 05	7	73	65	05	
Satie 5	1 11 12 13 14 15 16 17	18 10 10 10 10 10 10 10 10 10 10 10 10 10	78 81 83 81 78 70 70 67 63	27.150 29.230 29.260 29.270 29.310 29.310 29.330 29.330	300 100 350 360 360 360 010	15 12 10 10 10 12 12 10 10	***	57 59 62 61 63 64	940 74 68 69 70 63	10 98 11 12 10 07 06 08	000000000	57 58 59 57 57 57 57	883344449 999989	04 06 07 07 08 07 08	F F F F F F F F F F F F F F F F F F F	59 58 59	79 63 89	00 00 08	
June 10	20 21 22 23 24	65 61 57 55 56 54	56 65 59 66 62 72	29.420 29.420 29.430 29.430 29.430	170 110 230 .€0	07 06 06 03 05 04	A A A A	68 63 59 57	38 50 -7	05 03 00	000000	67 58	58 88	30 00 30	P P P P				

TABLE IV (Con't)

Date	Time EST	ESSA Weather Bureeu, Airpert				7. 934			P1e14			7 1016						
		7.	Nol. Num.	Po in. Ng.	Vind Dir. * Mag.	Vind Speed in	Pos	ī,	Rel. Hen.	Wind Speed kn	Pee	?	Rel. Num. S	Vind Speed in	706	÷p	Rel. Num.	Speed MIME
June 11	13 14	79	53	29.365 29.355 29.355 29.335 29.300 29.290	220	10	A	84 82	52 48	07	D				7	83 82		04 06
	14	79 80 76 79 79	53 49 58 58 63	29.355	220 230 230 230 230 230 230 230	10 11 10 08 06 05 06 05	! •	23	40	12 04 08 05	2				! !	12		06
	15 16 17 18 19 21 22	70	4	29.322	210	10	1 7	81 81	55 55 57	84	1 5			,				
	17	76	63	29.300	220	80	Ä	Ĭž	ŚŤ	05	ا م				,			
	18		6Ž	29.290	230	06	Ä				ÌĎ				7			
	19	76	67	29.290	230	05	A	77	65 59 70	03 00 00	D			03 00 06	7			
	Šä	74	69	29.300 29.300	230	06		76 75	59	00	D			90		78		00
	27	72	73	29.300	520	05	, A	75	70	90	D			06				
	22	70	\$2	29.300	230	96	A				۵				7	73		00

SAME V AIRCRAFT HOISE AND DISTANCE BATA

Poo	Date	Time	A/C	Materior Pt.	EPOL FFRA	SERVICE.	A-Joves .	9-10701 660	PRILA PROD	PHEAN PHE	PILC NLC	D 69	ě soc
A	5-17	1135 1141 1143 1213 1218 1219 1222 1405 1411 1432 1450 1509 1512	DC-9 727 BC-9 727 BC-9 727 BAC-11) DC-8 797 727 727 7580 VC-10	1572 1744 1438 2521 1586 2931 1653 2252 1975 1806	86.2 86.7 86.2 86.5 83.6 81.9 85.7 86.7 83.2 92.9	86.4 87.8 87.6 82.4 86.2 84.7 82.3 83.5 83.6 85.4 83.2	76.5 78.0 77.4 74.3 77.2 78.6 75.4 71.9 72.9 73.9 73.0 83.1	81.6 83.3 83.0 78.6 81.1 83.6 79.0 77.7 77.7 80.4 75.7	80.4 89.2 89.4 83.8 86.8 84.5 80.9 83.2 83.2 81.0 91.6	90.5 91.1 90.8 83.8 87.3 95.6 81.6 85.5 87.4 84.1 92.9	90.0 91.1 90.7 94.5 90.3 96.7 82.0 84.1 87.5 84.2 93.9	-2.3 -1.2 -2.1 -4.4 -1.1 -2.3 -1.4 0.3 -0.3 -0.7 -0.9	15.0 19.0 13.5 23.0 15.0 20.0 16.0 23.5 10.0 10.5 14.0 25.5
^	5-18	0611 0630 0645			105.4 83.1 90.0	98.0 81.5 87.6	91.4 72.4 78.1	100.1 77.2 84.0	104.4 83.1 90.7	109.8 83.9 91.7	105.4 84.1 91.4	-4.4 -0.8 -1.7	11.0 19.0 16.5
	5+18	0743700753700755710075571007557100755710075571008000822668200083682090009110121102277790473110053110053111043111243	707 720 727 727 727 727 727 727 737 727 737 727 737 727 72	227 3 1740 2365 1578 1577 1545 1616 1966 1526 1680 2305 2011 2078 1673 1731 1926 2570 3056 1954 2035 1954 2035 1954 1657 1829 1711 1652 1982 1657 1816 1801 1535	995-17698205955-65949415-176982086995-955-6594947-1731-698-845-1-1869942-6-998-7-1731-6-998-845-1-19747-198-998-845-1-19747-198-998-845-1-19747-198-998-845-1-19747-198-998-845-1-19747-198-998-845-1-19747-198-998-845-1-19747-198-998-845-1-19747-198-998-845-1-19747-198-998-845-1-19747-198-998-845-1-19747-198-998-845-1-19747-198-998-845-1-198-998-845-1-198-8-99	991.2792337092001121442695180938204785796862047857988998889888	84.4 4.4 79.63.6 972.9 972.6 882.9 972.9 882.9 97.7 97.8 97.7 97.8 97.7 97.8 97.7 97.8 97.7 97.8 97.7 97.8 97.7 97.8 97.7 97.8 97.7 97.8 97.7 97.8 97.7 97.8 97.8	92-3316 90-31-6 100-2-100 91-100-2-100 91-2-100 91-2-100 91-2-7-5-10 91-2-7-5-	95.1436.267.38.1.3.0857.5.4.9.8.7.6.6.0.1.7.38.1.3.08.957.2.5.4.9.8.7.2.5.4.9.8.7.2.2.8.7.2.2.8.7.2.2.8.8.8.7.2.2.2.2	101.68.4.27.86.8 7.4.4.6.4.5.0.2.6.4.6.9.98.100.6.89.100.6.89.5.89.100.6.89.100.6.89.100.6.89.100.6.89.100.6.89.100.6.89.100.6.99	100.96.68 105.68 105.11 105.12 105.13 105.13 105.13 105.13 106.13 107.15	-1.67:16.37.02.24.91.22.50.07.04.5.25.07.02.49.1.22.50.07.04.5.27.56.52.65.30.99.7.0.44.5.30.9.9.7.0.44.5.30.9.9.7.0.44.5.30.9.9.7.0.44.5.30.9.9.7.0.44.5.30.9.9.7.0.44.5.30.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.	16.0 15.0 15.0 10.5 13.7 11.5 12.5 12.5 12.5 12.5 12.5 12.5 13.0 14.5 14.5 16.5 16.5 16.5 16.5 16.5 16.5 16.5 16

TABLE V (Con't)

2	Date	Time	A/C	Distance Pt.	EPHL EPHA	STRL	A-level	D-level	PHEN	PHO	PNLC	D 4B	d 201
A	5-16	1134	580 DC-9	1816	95.8	84.0	76.9	79.5	85.0	88.5	87.0	-2.7	11.0
	i	1136 1146	DC-9	1781	92.5	88 .2	78.2	84.9	91.4	92.7	92.2	- ,2	20.0
		1200	727	1753 1567	92.2 94.4	88.5 90.7	\$1.6	99 .2	95.4	96.9 95.6	95.8	-2.7	9.5
		1212	Jet-Com	-50'	88.7	86.2	8 2.1 77.6	88.3 82.7	94.9	95.6	95.8	-2.5	15.0
		1215	727	2326	84.4	84.0	74.6	76.8	88.4 84.4	89.7 84.4	89.7 85.0	-1.5 0	19.5
		1219	DC-9	1354	94.8	90.3	82.2	90.3	96.7	99.3	97.9	-4.5	21.0 10.0
		1221	727 727	1526	96.6	92.7	83.6	6 9.5	96.4	97.9	97.9	-1.3	19.5
	ľ	1252 1254	727	1681 2053	90.2 88.6	86.9 85.7	77.3 76.8	83.7	90.1	91.5	91.1	-1.3	16.5
		1257	DC-9	1521	88.2	85.5	75.4	82.7 81.1	89.3	90.5	90.1	-1.9	15.0
		1314	707	1940	95.2	90.7	82.7	90.0	87.3 95.3	88.3 97.0	88.9 96.2	1	18.0
		1317	580	1880	83.1	82.4	75.2	76.8	82.5	85.7	83.6	-1.8 -2.6	13.5 12.5
	İ	1328 1409	DC-9 727	1900	91.6	87.7	79.0	85.9	92.3	93.9	93.3	-2.3	13.5
		1400	757	1905 2328	92.2 88.5	88.5	79 - 3	E5.6	92.4	93.9	93.6	-1.7	15.ó
		141,	727	1711	95.5	84.9 91.7	74.7	81.7	96.4	89.3	89.3	8	19.5
		1421	DC-P	1564	90.4	88.6	83.7 80.9	89.8 84.6	96.7	98.4	97.B	-2.9	11.5
		1427	VC-10	1570	95.3 89.2	93.9	85.5	99.9	99.7 96.1	92.4 97.1	,2.2	-2.0	14.0
i		1442	BAC-111	Suuv		97.3	79.9	64.5	90.0	91.2	97.3 90.7	-1.8 -2.0	17.0 18.0
		1444 1454	880 580	1442	35.6	34.3	85.6	99.1	95.6	96.4	96.7	8	15.0
		1500	727	1663 1731	92.7	85.9 88.9	77.9	79.4	85.3	99.5	67.1	-1.9	14.0
		1504	727	1633	65.6	86.7	78.6 77.1·	94.9	91.3	35.9	93.7	6	18.5
		1513	757	2132	171.1	177.1	99.1	83.4 94.3	99.1 199.3	91.5	91.2	-1.9	16.5
- 1		1515	580	1580	96.1	Ps A	77.3	79.7	85.6	101.0 89.1	101.3 87.0	;1	20.5
1		1516	720	1651	93.5	24.3	P5.0	94.5	9 . A	102.2	99.A	-2.0 -2.7	15.0 14.5
l		1527 1530	747 580	1032	23.3	30.9	P1.4	P6.2	95.9	94.3	94.9	-1.0	17.5
		1533	727	1547 1630	85.1 92.6	92.9 89.9	74.9	70.4	84.5	97.1	A5.7	-2.1	18.ó
		1536	727	1364	93.6	90.6	78.9 81.6	84.2 87.4	90.3	93.3	93.6	7	18.5
		153°	720	ić31	100.4	94.2	86.1	74.4	94.3 99.2	95.1	95.4	-1.4	18.5
		1537	727	1600	94.4	21.8	92.2	97.5	93.7	103.1 95.2	100.0 95.3	-2.3 8	12.0
		1541 1546	567	1654	67.٦	86.7	91.4	P2.5	éř.i	21.6	PQ.0	-3.7	17.5 11.0
I		1556	727 737	2014 2014	27.5	12.2	71.4	75.7	P] R	82.7	23.7	2	22.0
1		1677	727	2230	Р3.6 83.8	83.5 P2.8	73.5	77.9	93.2	84.2	94.0	6	20.5
ı		1619	CC-P	1626	96.4	72.1	74.0 32.7	7 8.7 Pq.9	84.3	84.3	94.9	- ,5	22.5
- 1		1614	707	1753	96.1	91.4	83.6	91.0	95.1 95.8	97.9 99.2	96.0 96.7	ć -2 . 1	18.5
Ī		1617	707	2010	<u> </u>	P3.1	72.1	76.5	62.4	94.3	94.1	1.0	14.0 29.5
Į.		162 8 1631	PAC-111 727	18fn 1933	82.3	A1.0	49.6	74.3	20.5	92.1	83.3	ž	26.0
- 1		1632	200	1521	85.5 86.6	P3. P P4.7	73.9	7º.0	24.0	84.9	R5.5	.6	25.0
- 1		1640	727	1546	94.5	21.	75. 5 91.7	91.2	P7.5	8A.0	80.2	-1.4	15.0
- 1		1642	707	1515	97.5	92.4	84.4	87.2 91.9	93.5 97.2	95.1 99.3	95.1	6 -1.8	18.5
ı		17~2	727	1818	100.3	93.5	87.2	95.7	100.6	105.5	97.9 101.6	-5.2	17.0 8.5
- 1		1737 180/	רפיז	2280	74.9	75.6	68.2	71.9	77.2	79.7	79.0	-4.8	10.0
		1813	727 727	1432 2100	86.9	86.1	77.8	82.2	98.2	\$9.0	88.7	-2.1	14.5
		1821	757	1644	#3.7 97.7	83.1 92.2	74.0	78.3	83.8	84.7	84.5	-1.0	18.0
1		1822	727	2320	87.1	84.9	93.9 75.2	91.1 80.6	96.5 86.9	100.1	97.5	-2.4	15.0
ŀ		1829	737	1675	89.5	86.1	76.0	82.9	89.0	87.8 27.9	87.9 90.0	7 4	16.5 19.0
- 1		1852	580	3201	80.1	78.3	69.4	72.4	78.3	81.0	79.6	9	26.0
ĺ		1855 1856	1:-33	j	69.6	62.1	60.2	67.3	71.0	72.4	77.2	-2.Ř	17.5
		1858	5-99 580	1680	67.2	6A.3	60.3	65.7	71.3	73.2	73.7	-4. ↑	11.5
	e 10				87.5	96.1	70.5	91.9	A7.6	9.00	88.8	-3.4	12.5
^	5-18	1907 1914	707 727	1581	105.1	98.3	89.6	99.3	103.4		104.3	-2.9	13.5
i		1915	580	1657 1645	92.7 87.3	88.7 86.3	79.2	95.7	92.4	93.7	93.5	-1.0	16.5
1		-/-/	,	- 7	01.3	90.5	79.9	82.5	88.5	91.2	89.4	-3.9	12.0

TABLE Y (Con't)

The state of the s

Per .	Date	Time	MC	Distance Pt.	EPIEL EPIEM	SERRI.	A-level	9-level	PHILM PHOS	PREEN PREED	PHILC	D 48	4 30c
A	5-18 5-18	1916 1918 1929 1932 1934 1937 1937 1939 1948 1950 1953 2005 2008 2016 2020 2020 2030 2030 2030 2031 2102 2119 2137 2139 2144 2151 2151 2151 2151 2151 2151 2151	797 727 727 727 980 727 727 707 8-80 727 727 DC-9	1742 1744 1600 2209 1337 1380 1572 1616 1837 2495 1639	98.4 92.5 93.1 88.2 91.9 101.3 70.2 81.3 90.4 100.5 93.5 92.4 102.3 93.9 94.7 95.1 94.7 95.3 94.7 95.3 96.3 96.3	922.25 88.77 89.00 97.6628 87.342148 970.887.342148 970.887.774866525 970.887.774866525 970.887.77487.77487.59997747.59999799999999999999999999999	84.5 740.5 7	22.2 23.8 26.8 270.3 26.3 270.3 24.6 27.5 27.5 27.5 27.5 27.5 27.5 27.5 27.5	98.6 93.1 93.6 84.5 90.4 100.8 71.3 81.3 91.6 91.6 91.1 93.3 100.5 94.7 93.3 94.1 93.7 95.9 94.7 95.9 95.9	101.8 94.3 95.2 05.3 91.7 107.8 72.2 83.5 85.5 70.6 94.7 87.0 103.8 895.4 95.1 107.8 97.2 94.5 96.9 107.8 97.2 107.8	99.5 93.9 93.9 94.2 85.1 92.1 102.3 73.1 82.9 92.6 101.6 93.8 101.3 95.4 95.4 95.4 96.3 97.9 94.8 95.4 94.8 95.4 95.5 96.3	-2.8 -2.12.7 -2.15.0 -2.15.0 -2.15.0 -2.15.0 -2.15.0 -2.15.0 -2.15.0 -2.15.0 -3.15.0 -	10.5 15.0 18.5 18.5 12.5 12.5 15.0 15.0 15.0 24.0 20.5 21.0 20.5 21.0 21.0 21.0 21.0 21.0 21.0 21.0 21.0
A	5-19 5-19	0642 0707 0745 0813 0838 0836 0850 0850 0850 0924 0924	DC-9 DC-9 720 727 DC-8 707 727 DC-8 727 727 727 37 727 3AC-111 Je -Com 727 Jet-Star	1795 2073 1508 1468 1851 2347 3135 1679 1744 1967 1415 2965 3019 1731	90.4 92.5 96.1 96.1 81.0 81.0 93.9 93.9 93.6 85.7 85.9	97.4 8559 91.53229 91.53229 80.294.659 83.653.95	77.0 77.9 84.2 84.0 85.2 75.7 72.4 83.3 81.2 76.4 79.7 76.0 78.0	90.2 83.6 85.3 92.8 91.7 90.0 76.7 91.1 81.3 86.4 92.0 81.2 84.9	76.1 89.8 91.8 97.9 98.7 85.1 97.5 87.5 87.8 98.8 98.8 98.8 98.8 98.8 98.8 98.8	96.1 89.7 93.2 102.0 99.8 86.9 82.5 100.8 88.1 90.1 85.7 91.8 87.7	96.7 91.3 92.9 98.7 98.9 99.3 87.18 99.0 95.4 88.0 90.4 90.4 90.0 92.3	-1.5 .7 6 -2.5 -2.9 -1.7 -1.5 -1.9 -2.2 -3.5 -3.0 -2.4	19.0 22.0 21.0 12.0 16.0 19.0 26.0 22.5 24.5 17.0 17.0 17.0 8.5 17.5 16.0
		0957 0959 1008 1012 1534 1537 1539 1541 1543	R-97 DC-9 580 727 DC-8 720 727 720 727 727 DC-8	1767 1736 1755 1679 1517 1645 1554 1798	78.3 94.0 86.8 95.1 99.2 103.4 103.4 103.6	74.7 88.9 85.9 90.2 92.7 96.5 89.4 96.9 89.7 93.5	67.5 79.4 78.8 82.0 83.6 80.0 89.7 80.2	74.9 87.3 80.5 88.9 91.8 97.4 86.3 98.5 86.2	80.6 93.4 85.4 95.7 97.8 102.5 92.9 102.6 99.6	81.9 95.0 88.2 97.5 101.2 106.8 94.0 106.6 103.3	82.4 94.5 87.6 96.4 98.9 103.1 94.2 103.8 100.4	-3.6 -1.0 -1.4 -2.4 -2.0 -3.4 6 -3.2 9	9.0 16.0 16.0 14.0 10.5 10.0 20.0 12.5 20.5

TABLE V (Con't)

Peo	Date	Time	A/C	Distance Pt.	RPHL EFFLOR	SENEL	A-level	D-level	PRES PAGE	PHERM	PMLC	8	
A	5-19	1549 1551 1552 1554 1556 1601 1609	727 727 BAC-111 DC-8 737 727 727	1657 1876 1654 1571 1351 2209 1966	94.6 92.0 89.2 101.8 95.3 90.0 92.1	90.6 89.4 87.7 95.7 90.9 87.2	81.7 79.9 80.2 85.9 82.6 76.6 78.5	88.2 84.9 84.2 93.6 99.9 82.5	95.2 91.1 90.0 99.7 96.3 09.2	96.9 92.2 90.0 102.6 97.6	96.1 92.5 91.1 100.7 96.9 90.6	-2.3 8 8 -2.3 9	12.5 18.0 18.0 18.0 15.5 20.0
A	5-19	2119 2128 2138 2141 2143 2146			98.3 84.5 96.4 88.8 84.6 94.9	93.4 83.2 92.3 85.9 84.4	84.8 74.1 83.5 76.0 75.4 81.6	92.5 78.4 90.0 82.1 79.5 87.6	91.4 97.4 84.5 96.5 88.3 85.0	97.5 99.4 85.7 97.4 89.9	92.6 08.4 76.1 93.0 89 85.0	4 -1.1 -2.2 -1.0 -1.1	18.4 16.0 16.5 17.5
^	5-19	2251 2148 2301 2321 2336			79.9 190.5 76.8 78.6 98.9	80.7 95.3 77.3 78.1 86.1	72.5 88.2 67.9 68.2 77.6	76.4 96.3 71.6 72.4 81.2	94.7 81.7 100.1 76.7 78.1 87.6	96.9 83.1 104.1 *7.8 79.2 91.0	96.4 84.7 101.6 78.1 79.5 89.6	-2.0 -3.2 -3.6 -1.0 6	14.0 15.5 10.5 23.0 26.0 16.0
A	5-23	0832 0834 0855 1004 1010 1010 1103 1103 1103 1103 1103 1143 1143 1143 1143 1143 1143 1143 1143 1153	BAC-111 727 BAC-111 727 DC-9 737 720 DC-8 720 DC-8 720 BAC-111 727 T-727 T-39 R80 747 727 720 DC-9 727 T-39 R80 747 727 720 T-39 DC-9 T-77 727 T-39 BAC-111 727 720 T-70 T-70 T-70 T-70 T-70 T-70 T-70 T-7	163° 1686 1813 1528 1810 1967 1591 1429 1418 1536 1676 1712 1606 1657 1612 1559 1554 1694 1621 2018 2111 1785 1720 1537 2017 1702 1657 1657 1668 2098	71898889;2554.1734196824 014432697414813553120467015185924173419687776 01518597414813553120	#7560261841176620462754 38574921873085737961514975793077776620462754 385749218730857379615149757930777766699749164	987802.6629530747564368 8906477787888699367 9877787833330747564368 890647778888699367777777777886427511009	### ##################################	93.7.9.3.6.6.0.4.5.9.6.5.1.5.5.3.3.6.9.1.4.5.9.6.5.1.5.5.3.3.6.9.1.4.5.9.6.7.4.0.4.6.1.3.9.6.9.1.4.5.9.6.7.4.0.4.6.1.3.9.6.9.6.6.9.6.6.9.6.6.9.6.6.9.9.6.6.9.9.6.6.9.9.6.6.9.9.6.6.9.9.6.6.9.9.8.6.9.9.7.1.3.9.8.8.8.8.9.9.6.9.9.8.8.8.8.9.9.7.1.3.9.9.8.8.8.8.9.9.9.9.8.8.8.9.9.9.9.9.9	95.6 96.8 91.8 95.2 88.6 97.2 84.6 98.0 109.3 89.1 100.3 89.1 100.8 100.8	9915.592315547.988888725.135478899.10347.6851813715138478899.10347.685181371513847899.10347.685181371513847899.103478887899.103478887899.1034788899988899988889998888999888899988889998888	-3.6 -2.1 -1.7 -2.5 -1.7 -2.6 -1.1 -2.7 -2.8 -1.1 -2.7 -2.6 -2.7 -1.5 -2.7 -1.5 -2.7 -1.5 -2.7 -1.7 -1.7 -1.7 -1.7 -1.7 -1.8 -1.1 -1.8 -1.7 -1.8 -1.8 -1.8 -1.8 -1.8 -1.8 -1.8 -1.8	13.5 13.5 18.0 23.0 16.0 23.0 16.0 21.0 17.0 10.5



TABLE V (Con't)

The second secon

Pos	Date	Time	A ∕€	Distance Pt.	EPNL Trace	SENEL	A-level CDA	P-love?	PHUN Phás	PHILEN Phies	MLC	D 48	4 .
A	5-23 5-23	1818 2009 2044 2114 2130 2140 2148 215° 215			67.1 09.3 77.6 04.6 78.5 77.9 83.1 04.9 99.8	86.3 89.6 77.0 82.6 79.2 77.6 82.9 85.0	76.5 79.8 68.3 72.5 66.3 68.5 72.8 75.5 85.4	81.2 83.5 73.0 77.5 72.0 73.7 76.9 79.6 93.8	67.3 88.9 78.6 82.3 76.8 79.2 82.2 85.0 98.9	87.6 89.8 79.0 85.5 77.6 30.0 81.4 86.5 103.5	87.9 90.4 80.1 84.1 78.8 80.6 83.1 86.5 99.8	5 -1.4 9 -2.1 3 -1.6 -3.7	19.5 19.5 16.5 23.5 23.5 13.5 23.0 21.0 9.5
^	5-23	220° 2219 2221			71.9 87.8 101.6	76.3 96.1 95.3	66.7 76.1 89.1	71.0 #1.1 97.1	76.0 87.3 102.2	78.3 89.1 104.6	77.6 88 6 102.6	-6.4 -1.3 -3.0	4.5 17 0 11.5
A	 24	1438 1445 1450 1551 1552 1522 1637 1663 1663 1644 1644	727 727 727 727 727 VC-10 747 729 DC-9 71LF :1 DC-9 707 727 737 DC-9 727 727 727 727 727 727 DC-9	1757 1450 1433 1730 1713 1673 1570 17700 1560 .718 1722 1725 1521 1717 1017 1045 1473 1720 1653	98.2 97.3 88.7 98.4 107.4 101.6 89.4 103.6 97.5 97.4 93.5 97.4 99.4 106.7	92.8 92.7 86.6 94.6 100.8 47.2 87.2 97.7 90.7 90.7 90.7 91.7 91.7 91.7 91.7 91.7	833-738-25-054-29-6-214-29-11-11-3	90.8 90.7 82.6 94.7 90.7 192.0 92.5 83.4 96.1 89.9 87.7 88.6 91.3 93.9	97.8 97.6 997.6 100.9 106.7 101.0 89.7 96.0 97.6 98.7 98.6 98.6 98.6 98.6	99.5 99.0 89.8 101.9 102.8 102.8 105	98.9 98.5 90.0 101.7 97.9 107.6 102.1 101.5 91.1 102.7 107.7 107.9 96.9 94.3 96.9 95.6 99.3 106.3	-1.37 -1.2.36 -1.2.36 -1.9.2.4 -1.7.58	16.0 14.5 21.5 22.5 12.0 17.5 15.5 15.5 15.5 14.5 13.0 13.0
A	°-25	79228 79228 79228 7928 7928 7928 7928 79	RAC-1:1 777 727 727 727 727 727 727 720 727 727	1703 1616 1676 1681 2209 1754 1555 1864 1735 1762 1589 1469 1478 1438 1601 1616 1305	#9.2 89.8 101.2 94.5 #5.5 90.7 #6.5 90.7 #6.5 101.6 96.8 100.5 93.4 107.7 96.1 176.8	97.5 97.1146 98.5 98.5 97.18 9	78.2.2.4 894 997 804 851 801 818 818 818 818 818 818 818 818 818 818 819	83.12 85.12 878 878 878 878 812 876 896 899 869 959 805 812 896 805	89.5274341013.34	90.5 92.3 105.3 95.3 95.9 90.7 87.9 90.7 87.8 90.3 103.8 109.9 96.8 96.8 96.8 96.8	90.1 91.8 94.8 93.0 95.7 93.7 91.7 91.7 98.0 100.5 94.6 94.6 95.7 97.0 88.9 97.0	-2.593.140.30.3884.5336.7684.9788	20.5 10.5 10.5 10.5 17.5 20.5 17.5 20.5 13.5 13.5 13.5 13.5 13.5 13.5 13.5 13
^	5-25	1900 1905 1912 1909			105.9 103.9 90.2 106.0	97.1 88.1 98.7	92.9 89.2 79.2 92.5	101.5 97.6 84.7 101.2	165.0 103.3 20.9 105.2	110.6 107.3 91.4 11J.5	106.7 104.3 91.6 106.1	-1.2	8.5 12.0 20.5 8.0



TABLE V (Con's)

2	Dete	7100	NE	Distance Pt.	RPSIL EFRAN	SECTION .	A-level	D-level	PHUN	PHILEH	MIC	D	-
^	5-25	1917			80.5				Price	71040	PHAD	48	4
1		1917 1914 1918 1925 1925 1929 1931 1938 2004			33:2	37.9 39.9 94.4	77.9 \$1.0	89.4 50.0	99.2 98.3 103.6 105.2 95.4 93.5 95.0 93.7 99.9	99.8	\$0.7	۵	20.5
		1025		1	103.1	94.4	41.0 95.1 91.0 92.5	91.8	98.3	95.8	95.1 99.5 104.4	٠٠,٤	14,5
ı		1929	- 1	1	105.4	37:1	91.0 92.4	91.8 99.4 101.8 86.9 88.4 87.0 85.3 83.6 83.6	103.6	108.1	104.4	-1.8 -5.0 -5.3	25.6 9.6
- 1		1931	1	j	77.0	92.2 90.3	2.4	98.8	95.2	110.7	304 1	-5.3	6.9
- 1		2004	· · · · · · · · · · · ·	ì	95.0	92.1	80.4 83.2 80.2	\$6.9	93.5	93.7	94.4	- ,5	27.
- [2005	ı		91. :	92.1 97.9	80,2	87.0	95.3	93.7 96.4 93.9	95.9	-1.4	21.9
- 1		2007	1	}	9.9	89.4 86.3	79.6	65.3	91.7	(5.2	94.0	-1.7 -1.0	13.5
- 1		2143	- {	ı	95.9	84.4	75.3	79.1	9.9	96.3	96.6 94.4 95.9 94.0 92.9 91.6 87.5	-2.2	15.0
1		2148	į	1	105.4 95.6 95.2 95.1 91.2 91.2 94.6 94.6 108.9	91.0 90.7	79.6 78.3 75.3 82.8 80.4	89.8	95.7	96.7	87.5	4	25.5
_1	_	2151	- 1	- 1	108.9	101.5	93.8	57.3 102.6	84.9 95.7 93.7 107.5 87.	96.7 94.7	96.5 94.5	-2.3 1	15.0
					83.9	P3.6	93.8 74.5	81.3	107.5 67.2	112.2 99.5	108.5	-3.3 -6.6	15.0

TABLE V (Con't)

Poe	Date	Time	A/C	Distance Pt.	EPHL EPHAB	SEMEL 49	A-level	D-level	PHEN PHEN	PHLTH PHAB	PMLC PMGS	D 48	d \$00
A	6-2	1501 1514	727 727	1333 1693	97.7	92.4	84.1	21.7	98.0	99.5	99.0	-1.8	15.0
1		1523	747	1649	92.9 96.3	89.4 94.3	82.0 85.4	88 .9 92.0	95.5 98.3	96.3 100.3	95.7 99.0	-3.4 -2.0	11.5 17.0
i	ł	1527 1529	DC-8 VC-10	1624	98.3 98.8	94.7	85.9 86.0	91.1	97.5	100.8	100.3	-5.0	16.0
l	ĺ	1531 1533	720	1571 1572	98.4	95.4	87.0 87.7	92.2	98.4	100.3 103.3	99.6	-1.9	18.0
l	ì	1533	727	1365	99.8 87.0	93.4 93.0	74.3	95.5 80.3	99.8 86.8	87.6	100.3 87.8	5 6	13.5 23.0
l	1	1535 1537	BAC-111 580	1773 1549	85.1 82.9	82.3 81.8	74.7 74.7	79.6 76.3	85.5	86.1	86.8	-1.0	15.5
l	ļ	1539 1540	580	1580	83.0	8 2.0	75.7	77.5	82.3 83.0	85.8 86.6	84.1 84.2	-2.9 -3.6	10.5 10.0
i		1540 1542	DC-8 DC-8	1612 1515	93.0 93.5	87.4 87.6	79.9 78.4	87.5	93.0	95.1	93.8	-2.1	11.0
1		1545 1555	727	1622	95.0	90.7	82.3	85.9 89.0	91.5 96.1	94.2 97.5	92.5 97.1	7 -2.5	17.5 14.5
•	İ	1555	720	1717	103.5	96.9	87.7	96.1	101.2	104.8	102.7	-1.3	17.5
İ		1557 1601	727 727	1578 1528	93.8 95.3	89.6 90.8	81.1 83.8	88.7 90.2	94.8 97.2	95.7	95.4	-1.9	15.0
1	ĺ	1604	727	1557	93.3	89.5	81.8	89.2	95.6	98.2 96.5	97.7 9€.0	-2.9 -3.2	17.5 11.5
	l	1615 1622	707 727	1590 1341	107.3 96.5	99.9 92.6	93.7	102.5	107.1	111.4	107.€	-4.1	11.5
	İ	1627	DC-9	1652	98.6	93.2	83.3 84.1	88. <i>(</i> 91.2	95.€ 98.4	97.2 9 9.8	97.5 99.8	7 -1.2	19.0 17.5
	i	1629 1631	727	1611	95.5	90.7	83.8	91.3	98.0	99.6	98.3	-4.1	11.5
] ;		1635	BAC-111 727	1703 1568	89.8 94.4	85.8 89.3	77.1 82.5	83.8 90.5	90.5 9€.5	92.1	91.3	-2.3	18.0
		1642	727	1639	97.2	91.6	8€.9	94.7	101.1	98.1 102.4	97.4 101.6	-3.7 -5.2	10.5 10.0
Α	1-3	0636 0639	720 DC-9	1631	98.4	93.0	84.3	91.5	96.8	100.2	99.0	-1.9	15.5
		0645	727	1824 1611	91.0 89.4	87.9 86.2	78.5 76.2	84.0 82.9	90.4 89.5	91.2 90.1	91.7 90.4	2	15.5 17.5
A	۱-5	0704 0711	D0-8 DC-9	1686	95.9 88.1	91.0	83.0	90.3	96.1	98.9	96.8	-3.0	
		2747	0C-9	1740 1689	97.4	84.4 92.2	74.9 82.9	82. 5 90.0	88.2 97.5	89.2	88.8	-1.1	15.5 16.5
		749 2753	720	1611	103.3	37.7	11.6	100.2	103.7	99.1 138.2	98.7 105.0	-1.7 -4.3	15.0
		1758	727 727	1589 1609	94.3 90.3	89.5 8 7.2	81.2 7 8. 1	88.7	95.2	7€.6	96.1	-2.3	13.0
		1303	727	1568	92.0	88.7	80.1	83.9 87.5	90.3 94.1	91.3 95.6	92.2 94.9	-1.0 -2.8	21.0 12.0
!		1326 1328	DC-9	1740 1560	95.3	90.6	81.8	89.5	96.3	98.1	97.4	-2.8	13.5
. 1		1342	DC-9	1900	94.6 90.2	90.7 87.0	80.7 77.3	87.1 84.7	93.9 91.1	95. 2 92.5	94.8	- ֻ.€	19.0
		13)	CC-9	1869	93.3 85.8	88.€	80.2	87.5	23.2	15.0	92.2 94.9	-2.3 -1.7	11.5 15.0
		1355 1401	737 BAC-111	2155 2263	85.8 85.4	83.5 84.4	73.1 74.7	79.1 79.1	93.9 85.1 84.4	gr.n	86.1	2	22.5
		1403	DC-9	1785	86.3	84.8	75.7	82.7	88.6	85.5 89.3	8€.2 90.0	1 -1.0	23.5 17.5
		1411 1414	70 7 720	1626 2310	105.9	99.3	02.2	101.0	105.7	108.7	106.3 96.8	-2.8	10.5
		1442	DC-8	2150	97.3 97.6	90.(97.0	82.7 87.8	91.0 92.4	95.7 98.1	99.6 9 8. 9	96.8 98.9	-2.3	13.0
		1455	727	1657	92.8	89.7	79.3	85.1	92.0	93.5	93.5	-1.3 7	16.0 22.5
		1505 1507	707 720	1712 172 8	103.7 97.2	96.6 94.0	89.1 85.2	97.6 90.6	102.7	106.7	103.6	-3.0	22.5 12.5
		1510	727	1856	88.2	85.8	76.4	82.7	96.4 89.0	98.6 89.8	98.5 90.1	-1.4 -1.6	17.5 15.5
۸ .	6-3	1900 1903			101.5	95.0	88.5	9€.7	101.€	105.7	102.6	-4.2	9.0
		1906		l	87.1 94.1	85.1 89.1	75. 8 79.7	81.2 87.0	8€.9 92.7	67.4 95.7	87.9 94.1	3 -1.6	21.5
		1910	l	ļ	92.2	88.2	79.2	86.3	92.6	93.5	93.4	-1.6	17.6 16.0
l		1919 1920	i		93.4 94.4	89.7 80.9	90.4	8€.3	93.2	94.4	34.2	-1.0	20.5
		1921		i	100.4	94.9	80.6 90.1	80.1 98.4	74.4 102.5	95.5 196.7	95.2	-1.1 -6.3	15.0
1		1924	i	Į	87.2	84.7	75.1	81.7	87.9	89.0	103.0 88.4	-6.3 -1.8	15.5
		1932	ļ	İ	92.8	89.4	80.6	88.3	94.3	95.3	95.0	-2.5	14.C

TABLE V (Con't)

Pos	Date	Time	A/C	Distance Pt.	EPHL EPHAB	88M21. 48	A-level	D-level	PHEN	PREATR PROB	PHLC	D 49	d Pos
A	6-3	1986 1954 1955 1956 1957 2004 2010 2032 2035 2047 2049			95.3 98.2 92.0 95.3 98.1 91.5 105.0 101.7 82.7 101.2 95.8	91.2 91.8 89.1 90.9 93.8 89.7 97.6 95.2 81.5 94.9	82.0 84.2 79.4 81.8 83.7 77.6 89.8 85.2 71.7 85.3 81.7	88.3 92.4 85.4 89.6 90.5 82.4 96.6 93.4 77.0 93.6	95.4 98.1 91.7 96.0 97.5 88.6 103.7 99.3 83.6 99.3	97.1 101.3 92.8 97.2 98.9 89.4 106.9 102.6 85.8 102.1	96.5 98.5 92.7 96.9 99.4 90.3 104.2 100.3 84.3 100.4	-1.8 -3.1 8 -1.9 8 2.1 -1.9 9 - 3.1 9	20.0 14.0 19.0 19.5 17.0 27.5 16.5 17.5 15.0 13.5
A	6-4	063 6 0630 0640	707 727 DC-9	1702 1536 1949	99.6 94.8 89.7	93.9 90.1 87.5	87.2 81.4 78.0	94.6 88.4 83.4	99.8 95.0 89.9	102.9 96.4	100.9 95.8	-3.3 -1.6	10.5 12.0
A	6-4	0717 07751 07751 07752 0806 0806 0806 08227 0835 0835 1555 1155 11113 11123 11423 11	720 DC-9 727 720 727 720 707 DC-8 707 727 727 727 727 727 727 727 727 727	2023 1740 16744 1544 1554 1578 1772 1773 15758 1634 16461 16461 16461 1657 1657 1657 1658 1658 1658 1658 1658 1658 1658 1658	100.1 39.7.7 87.7.6 93.6 91.5 99.8 91.5 91.5 91.5 91.6 91.5 91.6 91.5 91.6 91.6 91.7 91.6 91.7 91.6 91.7 9	988988998869174787111938067859928745605436669004856177752882525641931119380678599287456054366690048561777	877788174.5.2146292917389122549.0635984 77744.9648.887778815.2146292917389122549.0635984 77744.9648.8877778818884.8887884.888888888888888	997545288436886998039117946080209115870065131971299754528843688699808989898989888788888988898988872	98.84.12.95.8.998.8.72.8.71.6.32.0.87.1.4.4.37.2.7.4.6.0.9.6.6.3.0.2.3.6.0.3.9.8.5.3.9.9.8.4.1.2.9.9.8.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9.9	90.3 102.6 88.9 99.1 108.9 99.1 108.9 99.1 108.9 99.6 88.9 99.6 88.8 99.7 100.7 99.6 88.8 91.1 91.1 92.3 88.8 93.6 93.6 93.6 94.9 95.7 96.7 97.7 9	9 990.8962.2.2.4.5.7.83 29.2.7.2.6.6.8.9.0.0.9.4.9.4.0.3.4.3.0.1.2.4.5.4.2.8.4.37.31.5.9.2.7.2.6.6.8.9.0.0.9.4.9.4.0.3.4.3.0.1.2.4.5.4.2.8.4.37.31.5.9.2.3.4.5.4.2.8.4.37.31.5.9.2.3.4.5.4.2.8.4.37.31.5.9.2.3.4.5.4.2.8.4.37.31.5.9.2.3.4.5.4.2.8.4.37.31.5.9.2.3.4.5.4.2.8.4.37.31.5.9.2.3.4.5.4.2.8.4.37.31.5.9.2.3.4.5.4.2.8.4.37.31.5.9.2.3.4.5.4.2.8.4.37.31.5.9.2.3.4.5.4.2.8.4.2.8.4.5.4.2.8.4.5.4.2.8.4.2.8.4.5.4.2.8.4.2.8.4.2.8.4.2.8.4.2.8.4.2.2.8.4.2.2.2.2	-1.73832882695634615666526246197772866914688727 95447421 -1.3.68727 9544747421	15.5555555005cccc5c550ccco55555000550500550500555555005500

TABLE V (Con't)

Pos	Date	Time	A/C	Distance Pt.	EPML EPMAB	SENEL 48	A-level dBA	D-level	PHEAT PHEAT	PHLTH PHSB	PMLC PM48	D 48	4
A	0-5	2043			107.2	100.2	94.1	102.8	106.7	111.3 99.8 88.0	107.4	-4.1	9.0
	}	2048	ł	į.	96.7	91.2	83.2	91.1	97.7	99.8	98.6	-3.1	13.0
	1	2100	ł	i	\$7.1	54.1	73.0	79.9	85.2		87.5	9	23.0
	1	2104 2114	ł	i	29.1	93.2	86.9	94.5	99.3	102.6	100.0	-3.5	12.5
	l	2114	1	1	101.8	96.3	84.8	93.0	99.0	101.6	100.2	.2	20.0
	}	2119 2125	į .	Į.	101.4	94.3	85.8	94.2	100.4	103.7	101.2	-2.3	16.0
	1	2138	1	ł	95.7	95.4	89.9	98.6	102.7	107.9	103.8	-5.6	8.0
	!	2140	1	ł	93.7	90.7 87.8	83.0 78.6	90.4	96.1	98.9	97.0	-3.2	13.0
	ì	2142	į	1	96.1	91.3	80.6	85.8 88.1	92.2 94.5	93.0 95.9	92.9	-1.4	14.5
A	6-5	2208	l	İ	96.6	91.5	82.0	89.5	96.3	98.0	95.8	.2	23.0
	-	5555			90.9	86.ó	76.8	83.5	89.2	91.2	97.7 89.8	-1.4 3	16.0 19.5
A	6-6	0712	1	ļ	90.2	86.5	70.4	85.7	91.7	92.3	92.2	-2.1	15.0
		0745 0745	i	1	90.2	86.4	78.€	£5.7	92.0	92.5	92.6	-2.3	12.5
	ŀ		ļ	i	83.5	80.2	70.9	76.4	82.9	84.3	83.9	8	18.5
	ļ	0800 0800	l		94.1	89.6	80.4	87.7	94.1	95.2	95.1	-1.1	15.5
	!	0825	l .	1	36.4	91.3	82.€	89.9	95.5	98.1	96.4	-2.7	17.0
	l	0827	1	ļ	100.8	96.2	8€. 3	91.€	98.0	102.0	101.2	-1.2	17.0
	I	0830	1	1	96 2 98.6	91.3 92.9	83.€ 85.6	91.1	96.8	99.4	97.4	-3.2	13.5
		0937	ľ	1	83.0	81.0	72.5	93.2	98.3	101.5	99.1	-2.9	13.5
		554€			82.4	81.5	71.2	77.1 75.9	83.2 81.6	84.5	84.6	-1.5	15.0
	1	CC49	ł		90.1	8£.7	77.4	84.5	91.0	82.1	82.4	3	20.0
		3851	1	ł	86.8	84.5	75.3	80.3	86.3	92.3 87.0	91.9 87.6	-2.2	16.0
	}	1644	BAC-111	1933	79.9	79.7	76.7	75.2	8c.6	81.7	82.9	-1.2 -1.8	16.0
1		1654	DC-8	1740	101.4	94.9	87.5	96.3	102.0	105.3	102.7	-3.9	12.0
	1	1656	727	2607	82.9	82.5	70.5	75.2	80.8	81.3	82.7	1.6	8.5 26.0
		1711	720	2373	88.4	84.1	73.4	80.4	86.1	89.0	87.8	- ,6	23.0
	ĺ	1714	DC-9	1795	90.8	87.5	77.4	84.1	90.3	90.7	91.6	i ii	17.0
	1	1719	BAC-111	1811	91.3	88.6	79.6	85.4	92.0	92.5	93.0	-1.2	17.5
	}	1721	727	1841	88.5	85.7	76.4	82.7	89.0	90.4	90.5	-1.9	14.5
		1700	BAC-111	1811	85.0	83.6	74.2	79.2	85.1	85,€	85.0	6	16.5
	}	2000 2007	l		96.2	89.3	80.4	88.4	94.6	9€.0	95.3		13.5
		2007	i		99.4	97.6	87.7	93.2	99.4	100.1	100.1	- 17	18.5
		2021	1	1	93.3 95.0	89.6	80.1	87.1	93.5	94.4	94.5	-1.1	19.0
		2025	1		87.8	90.2 84.9	82.2	90.0	95.6 88.2	98.0	9€.3	-2.2	14.5
		2032		1	88.8	86.7	75.4 78.0	81.5	88.2	88.7	88.9	9	21.0
		2036	1		96.7	92.1	83.2	83.1 90.5	89.6	90.1	90.5	-1.3	15.5
		2038	j	•	69.3	05.7	77.7	85.1	97.1 91.0	98.0 91. 5	98.3	-1.3	14.5
		2041	1		94.5	89.5	80.7	88.3	95.1	97.3	91.6 96.1	-2.5	16.0
		2102			93.5	89.ó	79.4	86.7	93.4	94.8	94.4	-2.8	13.5 18.5
		2103	1 1	ļ	85.9	84.5	73.6	78.7	84.4	85.6	85.6	-1.3	10.5
1		2118]		101.6	94.9	87.3	95.5	100.1	103.2	101.2	.3 -1.6	28.0 14.5
		2133	1		101.1	95.1	86.7	94.5	99.8	102.1	100.4	-1.0	18.5
- 1		2141	j		103.2	96.3	89.2	97.8	102.3	106.6	103.2	-3.4	13.5
- 1	Ì	2144	}		97.1	92.6	82.7	90.3	96.9	98.1	98.2	-1.0	18.0
- 1		2147			97.5	92.4	83.5	91.3	97.6	97.6	98.5	1	18.5
		2149	1		100.1	95.0	85.6	92.8	100.0	101.6	101.3	-1.5	18.ó
i		2153	 		92.9	90.0	80.0	85.7	91.7	91.7	93.5	1.2	25.0
A	6-6	2203	į		90.0	86.8	77.1	83.4	89.8	90.0	90.4	0	22.5
		2205	i		89.0	86.8	77.1	82.2	88.3	88.8	90.2	۶.	18.5
A	6-7	0017	720	1434	102.7	96.1	89.5	98.0	103.1	107.0	103.9	-4.3	12.0
1		0643	580	1612	87.4	85.8	79.6	81.4	87.1	89.8	88.6	-2.4	14.0
l		0648	DC-9	1701	90.9	88.0	79.1	86.3	92.3	93.0	93.3	-2.1	14.5
		0654	580	1646	87.3	85.9	78.2	81.0	87.2	90.5	88.6	-3.2	14.6

TABLE V (Con't)

Pos	Date	Time	A/C	Distance Pt.	rpnl Epnab	Senel 49	A-level	D-level dBD	PHLM PHGB	PHLTM PHAB	PNLC PNdB	D dB	d sec
A]	6-7	C703	58c	1717	87.6	85.5	76.8	79.4	85.6	89.5	87.1	-1.9	17.5
		0707	DC-8	1664	99.0	92.7	83.3	90.8	96.7	99.9	98.4	9	16.5
	i .	0745	DC-9	1781	92.8	68.1	79.3	86.9	93.1	94.3 108.8	94.0	-1.5	17.5
	l	0754	725	1554	103.8	97.7	92.4	101.1	104.2	108.5	105.7	-5.0	8.0
	i	0756 3800	720	1764	91.7 100.5	88.4 94.7	79.0	84.8	91.6	92.8	92.8	-1.1	21.0
	l	0803	127	1731	88.9	86.0	87.4 76.6	95.5	99.5 89.5	102.9 90.4	100.6 90.6	-2.4 -1.5	16.5
	}	0807	707	1663	104.1	97.5	92.8	83.3 101.4	105.4	110.0	106.3	-5.9	15.5 8.5
	ŀ	0813	737	1534	86.7	86.1	75.0	81.7	87.7	88.2	89.2	- 7.5	23.0
1	ì	3819	707	1534 1582	95.6	93.9	85.7	93.0	98.7	99.9	99.6	-1.j	14.0
	1	0828	Lear	1621	91.2	89.9	81.0	85.3	91.1	91.8	93.4	6	20.0
	ļ	0821	720	1332	109.0	101.8	95. 8 87.9	104.6	109.1	113.8	109.6	-4.8	8.5
	1	0830 0832	707 DC-8	1890 1680	101.3	95.5	87.9	96.2	100.5	104.3	101.7	-3.0	15.0
•	{	0835	727	1357	97.5 97.0	92.1 91.9	81.7 83.0	89.0 90.0	75.6 06.0	99.4 98.1	97.7 98.0	-1.9	16.5
	Į.	0844	727	1333	82.6	81.0	70.2	75.3	81.4	82.4	82.5	-1.1	15.5 24.0
	ĺ	0845	580	1859	86.7	24.6	77.3	79.6	85.5	88.4	87.0	.2 -1.7	16.5
j '	1	. 849	580	1596	27.8	86.3	79.3	9.06	96.3	E9.1	88.9	-1.3	14.6
ľ	l	0851	CC-9	1701	92.4	89.0	78.9	86.3	92.9	94.0	93.6	~î.€	16.5
]		0854	737	1534	94.6	90.6	79.8	P7.3	93.6	94.0	94.5	3	23.5
Í.	ļ	6855	727	1871	88.7	85.5 83.8	76.9	82.7	89	89.7	90.3	-1.0	18.0
	Į	0912	: AC-111	1703	86.1	83.8	75.7	80.2	86.7	87.8	87.7	-1.7	17.0
	[0925 0925	BAC-111 727	1654 1478	92.0 91.1	89.0 89.2	8C.9 79.6	86.f 84.7	93.3	94.8	04.0	-2.8	15.5
,	1	0934	720	1591	101.7	36.2	91.2	29.5	91.2 102.8	91.8 106.5	92.1 103.5	7 -4.8	16.0 9.0
		0936	727	1657	93.4	88.7	81.5	áέ.ϵ	95.3	96.7	95 A	-3.3	13.5
		0941	AI.C	2334	82.5	80.3	72.0	76.7	81.7	83.9	95.8 83.6	-1.4	27.5
	}	3944	737	1560	87.9	85.2	75.4	81.3	87.5	88.3	88.8	4	18.0
{	Į	1063	580	1795	86.5	85.3	78.5	80.2	85.9	89.2	87.7	-2.7	12.5
1	ļ.	1/11 1012	DC-9	1701	97.5	91.8	83.6	91.2	98.1	99.8	98.9	-1.3	14.5
)	ľ	1012	727	1357	93.8	90.1 88.5	81.2	87.6	94.9	96.5	96.0	-2.7	18.0
1	ļ.	1015 1014	FAC-1:1 727	1509 1381	91.3	87.5	81.4 78.3	86.6 84.8	92.9 91.€	93.4 92.5	94.0	-2.1	17.2
1	ŀ	1023	. 580	1540	éê.	91.2	60.5	A2.5	29.4	92.7	92.3 89.5	-1.4 -3.2	18.5 12.5
l	l	1027	DC-9	2192	88.5	85.9	77.9	84.1	90.5	90.5	91.0	-2.0	15.
1	ì	1033	727	1450	94.8	90.4	82.2	89.5	96.3	97.7	97.0	-2.9	12.5
}	ļ.	1035			93.7	89.3	79.9	87.4	93.9	94.5	94.7	-`.é	20.0
1	Ì	1037	DC-8	1572	98.6	53.5	83.0	91.0	97.0	101.0	99.5	-2.4	15.5
l	l	1040	1		90.0	86.5	77.2	83.7	89.8	91.7	91.3	-1.7	16.5
(ł	1750	207	1274	94.3	89.7	81.5	88.1	95.4	97.0	96.1	-2.7	14.0
[1	1052 1054	707	1774 1574	102.4 94.8	95.3 90.1	87.5 80.8	95.8 8 8. 8	101.7 94.6	105.0	102.2	-2.6	16.
1	1	1102	DC-9	1802	89.9	86.3	77.1	84.6	90.6	95.7 91.1	95.7 91.1	9 -1.2	10.€ 15.€
1	Į.	1104	727	1611	96.7	91.6	83.1	90.4	97.3	98.8	27.9	-2.1	13.5
ì	1	1106	DC-8	155° 162	102.8	95.6	57.5	91,1	162.6	105.5	102.7	-2.7	14.4
1		1108	727		101.5	96.6	86.2	92.9	100.3	102.0	101.9	5	19.0
	i	1110	720	1517	103.9	97.6	92.8	101.3	105.0	109.1	105.9	-5.2	8.0
1		1115	DC-8	1680	86.1	84.1	76.5	79.9	86.5	88,9	87.6	-2.6	13.0
}	1	1120 1125	707 737	1796 1460	105.5 91.7	98.1 88.1	91.5	100.4 94.8	105.1	109.1	106.4	-3.6	11.0
]	ł	1127	586	1564	88.8	86.6	78.0 81.0	83.8	90.9 89.9	92.0 92.9	92.4 90.8	3 -4.1	17.5 16.0
1	i	1129	DC-9	1701	92.2	88.5	77.7	84.3	90.8	91.5	92.3	.7	24.0
}	1	1138	1	1	86.5	84.3	73.9	80.4	86.0	87.2	68.4	- :7	19.0
1]	1144	727	1634	88.8	85.9	77.2	84.1	90.2	90.9	90.8	-2 1	1€.n
l	l	1151	DC-9	1740	93.6	89.3	80.6	88.1	94.5	95.8	95.5	-2.2	13.0
l		1156	727	1669	99.1	94.1	85.0	92.0	99.2	100.8	100.4	-1.7	14.5
<u> </u>		1201 1209	DC-9	1689 1740	95.9	90.8	82.7	90.4	96.7	98.1	97.1	-2.2	15.0
!	1	1210	727	1547	98.5 97.4	93.1 92.3	83.6 94.8	91.1 92.9	97.8 99.7	99.8 101.3	99.4 100.4	-1.3 -3.9	18.7 12.0
ļ	I .	1210	1 ' - '	1 • • • • •	, ,,,,	74.3	07,0	76.7	-9.1	101.3	100.4	-3.4	4

TABLE V (Con't)

Pos	Date	Time	A/C	Distance Pt.	ephil Ephab	Semel 43	A-level dBA	D-level dBD	PHLM PM4B	PHLTM PHGB	PHLC	D dB	4 800
A	6-7	1217	Jet Ster	1622	94.1	92.6	86.3	91.6	97.3	98.0	98.1	-3.9	11.5
1		1220	727	1557 1657	94.3 97.3	89.9	84.4	91.5	98.0	99.3	98.5	-5.0	9.5 14.5
		1225	727	1657	97.3	92.5	84.8	92.3	98.6	99.1	99.1	-1.8	14.5
1		1232	DC-9	1701	95.4	90.3	81.5	89.9	96.5	98.5	97.4	-3.1	13.0
		1237 1240	BAC-111 580	1654 1505	90.2 91.1	86.7 88.8	78.0 81.8	84.6	90.8	91.3	91.7	-1.1	16.0
		1253	727	1706	92.8	88.9	80.5	83.9 88.2	90.4 94.3	93.K 95.2	92.4 95.1	-2.5 -2.4	12.5
		1311	580	1463	80.8	86.6	79.0	81.7	88.0	90.6	89.7	-1.8	13.5 12.5
		1324	DC-9	1932	90.8	86.6	78.8	85.5	92.1	93.7	03.7	-2.9	15.0
		1325	580	1681	86.1	84.2	78.9	81.0	87.7	91.0	93.1 88.2	-4.9	11.0
		1326	DC-9	1932	88.9	85.5	76.5	83.7	90.0	90.6	90.4	7	17.5
		1329	737	1508	90.0	66.2	78.7	66.0	92.0	92.3	92.2	-2.3	15.5
	İ	1340	DC-9	1839	92.8	88.5	80.7	87.9	94.3	95.1	95.2	-2.3	12.0
	ł .	1345	727	1441	84.4	86.6	76.9	82.4	89.1	89.4	90.0	-4.5	19.5
		1349 1351	DC-9	1731	92.0	87.8	78.3	85.8	91.9	92.5	93.0	5	21.0
		1351	580	1580	88.6	86.5	80.7	82.7	89.0	92.1	89.9	-3.5	10.5
	ł	1355	T-39	1784	81.1	79.0	70.7	75.8	81.1	84.6	83.1	-3.5	11.5
i		1401 1403	DC-9 DC-9	1735 2036	92.1 91.3	88.1 87.1	80.1 78.2	87.4 85.6	93.7	94.2	94.5	-2.1	13.5
		1408	727	1622	94.2	89.4	81.5	88.8	92.0 95.3	93.2	93.1	. 2.3	14.0
		1414	DC-8	1661	102.9	95.8	89.9	99.0	104.1	96.7 107.5	95.9 104.5	-2.5 -4.€	14 5
		1416	707	1672	105.6	98.7	91.5	100.2	105.1	109.9	105.8	-4.0	9.0 7.5
		1418	737	1574	95.6	90.9	82.1	89.2	95.3	96.2	9€.2	6	19.5
		1419	727	1681	93.0	88.9	81.2	88.7	94.9	95.7	95.5	-2.7	12.5
		1421	DC-9	1839	89.5	85.0	76.1	83.7	90.2	91.8	90.7	-2.3	15.5
		1423	LC-8	1867	97.8	92.0	82.7	91.0	97.3	99.9	98.0	-2.1	13.0
	ł	1425	b-80	253€	85.3	80.8	71.1	79.0	85.5	£7.3	87.5	-2.0	17.0
		1430	727	1657	97.9	93.4	83.6	90.5	85.5 97.8	99.3	99.4	-1.4	17.0
		1432	DC-9	1810	92.0	88.3	79.8	87.3	93.8	95.0	94.8	-3.0	13.0
	i	1437	DC-8	1751	99.2	92.9	84.7	93.1	99.0	102.4	99.6	-3.2	34.0
	l	1444	DC-9	1395	90.2	87.0	77.9	83.7	90.4	90.7	91.9	5	16.5
	f	1448	727	1381	93.8	89.2	83.0	90.3	96.8	98.2	97.1	-4.4	11 0
	ļ	1458	Lear	1720	84.5	83.3 94.5	74.7	79.7	85.7	86.3	8€.8	-1.8	14.5
	1	1503	VC-10	1579	97.4 87.6		84.1	90.0	96.0	97.9	97.9	5	17.5
		1507 1509	727 727	1785 1578	93.6	85.8 89.6	7 8.3 82.8	8 2.9 90.3	89.1 96.7	89.7	90.0	-5.1	14.0
		1511	727	1622	93.0	88.9	81.4	88.3	94.7	98.0 95.8	96.9 95.3	-4.4 -2.8	10.0
		1513	580	1564	84.4	82.4	74.2	77.6	83.7	86.0	85.5	-1.6	13.5 14.5
		1515	8-80	2290	79.6	75.5	66.6	75.5	81.5	83.3	83.3	-3.7	11.5
	Ī	1516	BAC-111	1670	88.0	85.6	77.6	82.7	88.9	89.5	89.5	-1.5	18.5
		1518	T-39	1649	84.7	83.8	75.6	78.4	84.6	86.3	8É, 2	-1.f	15.c
		1520	580	1463	89.7	88.2	84.6	86.8	92.3	96.0	93.0	-€. 3	6.1
		1524	707	1635	106.5	99.4	92.8	101.7	106.1	110.8	10€.7	-4.3	€.•
	l	1526	720	1631	98.7	93.4	83.7	90.6	97.0	101.1	99.3	-2.4	17.
i	ł	1529	747	1885	96.6	92.8	82.5	88.	95.2	97.6	96.1	-1.0	20.5
		1530	LC-9	1520	86.2	84.2	75.9	81.4	87.6	87.6	88.1	-1.4	50.6
		1533	580	1505	87.0	85.5	76.8	79.3	85.5	88.1	87.0	-1.1	18.C
		1537	DC-8	1726	97.1	20.8	83.8	91.7	97.4	100.0	97.f	-2.4	15.C
		1540 1544	727	1365 1669	91.0	87.4 89.€	77.9	83.8	90.5	21.7	91.7	7	19.
		1545	720	1763	93.7	92.8	80.4 87.2	87.8 95.3	94.3 99.0	94.7 101.4	95.0 100.0	-1.0 -2.5	45.5 15.5
		1547	BAC-111	1686	89.7	85.8	78.2	85.0	91.7	93.5	92.6	-3.8	12.5
		1549	DC-8	1581	26.4	91.7	82.7	90.9	96.8	99.7	97.8	-1.3	17.5
	1	1551	586	1717	88.5	87.3	81.3	82.3	88.6	91.4	99.8	-3.4	11.
		icci	720	1662	101.2	94.8	89.1	37.6	102.7	105.7	107.7	-4.7	14.5
		1553 1554	727	1578	92.3	88.4	79. ê	87.1	93.5	94.6	34.3	-2 :	13.6
		1558	127	1758	94.7	90.3	81.1	88.2	95.0	95.€	96.5	-	1/1
		1612	737	1484	89.5	86.1	77.4	84.5	90.7	92.1	91.2	-2.€	17 5
	Ì	1614	υč-2	1594	98.0	92.9	85.4	42.9	99.8	101.3	100.6	-3.3	12.
		14.14	30-9	1594	1 90.0	92.9	07.4	42.9	49.8	101.3	10€.€	-3.3	

TABLE V (Con't)

os	Date	Time	A/C	Distance Pt.	rpml rpmab	SEMEL 48	A-level dBA	D-level dBD	PHILM	PHLTH	PKLC	D dB	d 80 0
A	6-7	1617	727	1589	97.5	92.5	83.8	90.6	97.7	99.2	99.1	-1.7	15.0
		1622 1625	707 727	1830	97.0	90.9	84.4	91.7	97.3 94.6	101.1	97.7	-4.1	9.5
		1627	727	1731 1526	94.2	89.9	81.0	88.4		94.6	93.6		19.0
		1629	BAC-111	1870	91.2	88.6 88.4	79.5	85.8	92.3	93.0	93.1	-1.8	14.5
	+	1633	DC-9	2036	93.3	88.4	79.7 81.0	84.9 88.6	91.1	91.7	92.5	-1.6	17.5
		1634	720	1706	101.6	95.8	91.8	100.2	95.3 103.5	96.7 107.8	95.6	-3.4	12.5
		1644	727	1459	99.1	94.2	65.9	92.7	100.0	107.0	104.6 101.0	-6.2 -2.9	7.5
		1707 1728	727	1208	96.8	92.1	84.5	92.1	98.6	100.0	99.7	-3.2	13.5 15.0
		1729	707 707	1672 1743	101.2	96.0	89.3 90.8	97.2	101.1	103.8	102.0	-2.6	13.5
1	l	1731	727	2000	105.9 87.4	98.8 85.4		99.4	104.6	108.8	105.6	-2.9	13.ó
- }		1732	DC-9	2073	93.3	88.6	75.6 79.4	81.3	87.4	88.7	88.3	-1.3	21.0
- 1		1735	Jet Star	1806	90.8	89.8	81.5	86.5 85.8	93.3	94.6	94.3	∘1.3	15.5
- 1		1736	BAC-111	1830	92.0	89.3	79.9	85.0	91.5 91.3	91.5 92.0	92.7	7	17.5
- 1		1741	707	1617	99.2	93.3	87.1	34.9	99.2	101.9	92.9 99.9	-2.7	23.0
I		1743 1746	BAC-111 DC-8	1720	91.6	70.4	81.7	8.8	92.6	93.3	93.3	-1.7	14.5 16.0
		1755	720	1652	100.7	of . 2	85. 9	91.3	98.1	100.8	100.1	1	21.0
- 1		1757	727	1491 1676	194.7 88.9	28.2	12.3	100.9	105.1	109.5	106.0	-4.8	8.0
- 1		1757 1800	727	1536	96.2	85.4	76 4	83.6	89.4	90.2	90.0	3	17.5
- 1		1839	727	1415	96.4	91.7 91.8	83.1 84.0	90.9	97.3	98.7	98.0	-2.5	14.5
- 1		1:1-	LC-9	1839	98.0	93.1	83.4	91. 5 90.6	97.7	94.4	98.1	2.0	14.5
ı		161,	727	1333	97.4	94.5	Ĕ5.2	90.3	97.4	9 8.€ 9 8.1	98.3	6	18.5
1		1650	58C	1549	88.7	87.4	8ó.e	έ3.3	97.1 88.9	92.4	98.6	7	23.0
ı		1841	797	1565	109.0	101.3	9.30	105.6	109.7	115.2	89.6 110.5	-3.7 -6.2	11.0
i		1845	PAC-111	1623	87.7	86.1	76.6	€1.6	87.6	86.3	88.9	6	7.0
- 1		1847	737 580	1448	89.8	85.9	75.8	82.4	89.3	91.5	90.8	-1.7	16.c
ŀ		1850	737	1549 1460	88.4 97.2	87.7	80.5	82.1	87.€	20.3	89.0	-1.9	14.
- 1		1964	720	1483	101.3	92.2 95.4	81.3 86.9	88.7	95.3	96.3	96.8	. 9	24.5
- 1		1905	707	1712	102.3	95.8	91.9	100.4	99.5	103.1	100.6	-1.8	17.5
- 1		1907	580	1904	87.5	96.0	79.2	81.6	104.6 87.6	109.0	105.1	-6.7	6.5
- 1		1910	580	1534	89.5	88.2	8ó.8	83.3	89.1	90.8 92.3	97.9 90.4	-3.3 -2.8	11.0
- 1		1714	727	1389	91.0	80.3	78.4	84.5	90.9	91.9	92.0	9	12.0 18.0
- 1		1916 191 8	DC-9 580	1652	93.5	89.6	8 1.0	88.7	94.6	95.5	95.4	-2.0	15.5
-]		1920	727	1580 1268	88.8	88.5	83.4	85.0	90.7	94.5	91.5	-5.7	6.0
- 1		1926	UC-9	1727	93.1 98.0	89.4	80.7	87.0	93.8	94.8	94.6	-1.7	17.0
- 1		1928	727	1744	94.7	92.7 90.3	81.9 80.2	89.4	96.4	98.2	98.0	2	21.0
- [1929			99.9	94.4	86.3	87.9 93.9	94.3	96.0	95.7	-1.3	19.5
		1931	727	1547	96.3	91.7	82.4	90.0	99.3 96.8	101.9 98.7	100.1 98.4	-5.0	13.5
- 1		1933	727	1311	100.0	95.5	86.1	92.8	99.9	101.2	101.0	-2.4 -1.2	13.0 18.0
- 1		1935	DC-8	1720	102.0	95.2	86.8	95.6	100.9	104.1	101.9	-2.1	14.0
- 1		1937 1939	DC-8	1544	105.6	98.1	89.7	98.3	104.1	107.8	105.0	-2.2	17.0
- 1		1944	- 1	l l	92.7	88.4	78.1	85.5	91.8	93.0	92.9	3	16.5
- 1		1947			95.1 84.0	90.9 82.4	83.3	90.6	96.3	98.6	97.7	-3.5	12.5
- [2141	1	- 1	91.2	87.8	75.2 78.3	77.8	83.8	86.6	85.5	-2.6	16.C
- 1		2143			94.8	90.8	81.8	85.0 89.6	91.5	92.0	92.0	8	16.5
- 1		2148	j		89.8	85.9	75.3	81.8	95.5 88.3	96.3 90.1	96.4	-1.5	20.0
- 1		2150	1	į	97.7	92.0	82.8	90.3	95.1	89.8	90.5 97.3	3	21.0
-		2152	•	1	92.0	88.2	79.2	86.6	93.3	94,5	94.1	-1.1 -2.5	20.0 16.5
- 1		2154	i	İ	85.1	83.6	74.1	80.0	85.4	86.1	86.6	-1.0	16.0
- 1	6-7	5506	į	1	101.7	95.6	88.6	26.7	100.7				
i		2248	Į.	j	90.5	87.3	76.7	83.7	90.2	103.9 91.0	101.9	-2.2	12.5
		2302	- 1	1	95.6 98.4	91.1	81.1	87.5	93.7	96.6	91.6 96.1	5 -1.0	16.0
- 1		2309	1	1		92.2	83.6	91.6	97.3	100.2	98.1	-1.8	17.5 14.5
- 1		2332	i	T t	97.5	91.9	84.4	91.9	97.1	100.7	98.4	-3.2	12.5

TABLE V (Con't)

Pos	Date	:/she	A/C	Distance Pt.	EPHL EPHAB	881181 48	A-level	D-level	PHILM PHAS	PHLTP	PMLC	D	4
•	6-8	0051 0905 0905 0913 0922 0925 0930 0934 0943 1000 1010 1024 1025 1026 1037 1044 1046			86.4 82.3 83.7 83.7 84.2 84.1 85.8 89.6 87.3 81.1 103.2	82.9 81.4 83.2 86.2 88.5 84.5 82.8 83.3 83.3 85.2 85.2 87.5 85.2 80.1 97.4	75.6 73.4 74.5 74.9 76.5 72.9 76.5 73.8 73.9 76.1 75.4 75.1 75.1 76.5 71.1 93.3	82.4 77.9 77.9 78.9 78.0 78.4 78.4 79.1 79.9 85.1 86.3 86.3 86.3 76.3 80.2	89.0 85.2 84.2 84.5 88.6 63.5 84.5 84.5 84.5 84.5 85.0 91.1 86.0 91.2 93.0 93.0 93.0 93.0	904.792.965.5994.0995.944.91.094.91	89.2 86.2 85.4 85.4 85.4 85.4 85.4 85.4 85.3 85.3 85.3 85.3 85.3 85.3 85.3 85.3	-2.6 -2.2 -3.7 -2.3 -2.3 -2.3 -2.3 -1.1 -2.9 -1.3 -1.3 -1.3 -1.3 -1.3 -1.3 -1.3 -1.3	10.0 12.0 13.5 12.5 10.0 10.0 16.0 15.0 15.5 17.0 6.0
A	€-13	1911 1916 1918 1918 1919 1932 1932 1933 1947 1956 2011 2035 2045 2045 2113 2113	DC-9 727 707 727 EC-8 727 DC-8 DC-9 727 727 727 DC-9	2651 1771 2445 1917 2153 1798 1598 2171 1478 1871 2667 1681 2151	82.3 88.8 95.6 90.9 85.6 93.8 93.8 88.9 88.3 928.7 87.2 93.8	82.97886.991.670.28 84.51.070.28 87.082.065.1070.881.082.065.1	72-1 75-9 82-2 76-4 78-1 74-5 82-0 81-1 77-2 76-2 78-3 81-1 84-9 76-1 89-6 82-9	76.2 88.8 81.2 79.4 190.1 85.7 82.7 82.7 82.7 82.8 80.0 97.8 80.0 97.8	81.68 95.12 95.14 85.46 91.0 93.0 93.2 97.51 87.12 98.8 97.6 98.8	82.2 89.1 97.6 87.6 87.6 85.7 99.6 92.0 90.3 89.6 87.7 93.9 100.6 87.7	7.8.9.3.98.0.1.4.4.58.9.90.5.4.9.2.1.9.3.98.0.1.4.5.8.9.90.5.4.9.2.1.9.3.90.1.9.3.1.	-1.7 -2.2 -1.7 -3.6 -3.1 -2.7 -1.7 -1.3 -1.3 -1.3 -1.3 -1.3 -1.3 -1.3 -1.3	24.55.50.50.50.50.50.50.50.50.50.50.50.50.
A	€-11	1402 1403 1411 1435 1440 1450 1522 1531 1632 1653 1653 1732 1736 1739 1802	DC-9 DC-9 T27 DC-8 727 VC-10 720 DC-9 707 727 DC-8 DC-8 T27 DC-9 727	2092 2133 2000 1899 2667 4070 2462 2510 2171 2064 2829 2691 1830 2417 2780 2522	91.1 96.05 95.7 95.7 83.4 96.2 963.9 95.5 85.2 95.6 85.2	87.3 83.3 85.3 84.6 87.8 87.8 891.2 891.4 891.4 891.4 891.4 891.4 884.8	79.4 74.6 80.6 73.7 87.3 87.3 88.3 78.3 60.9 80.5 71.0	86.5 81.5 82.3 88.4 60.2 77.5 91.6 87.7 91.7 85.7 85.7 87.2 88.0 77.2 81.8	97.3 88.5 946.3 862.4 97.7 996.6 998.7 996.6 998.8 968.8 968.8 968.8 968.8 968.8 968.8 968.8 968.8 968.8 968.8 968	9478 9478 9478 9478 9478 9489 948	93.4 87.6 89.6 87.4 95.4 84.7 93.6 93.4 95.7 84.3 95.7 84.3 95.7 84.2	-3.4 -1.9 -1.7 -2.1 -2.1 -2.7 -2.7 -2.7 -1.2 -2.5 -1.4 -2.7	14.5 17.0 16.5 16.5 17.0 21.6 14.5 14.5 14.5 18.5 16.6 23.6 21.6 23.6 24.6 24.6 25.6 26.6 26.6 26.6 26.6 26.6 26.6 26

TABLE Y (Com't)

Pos	Date	Time	A/C	Distance Pt.	EPHL EPHAB	Samet.	A-level dBA	D-level dBD	PHEN PHEN	PHLTM PMAB	PHLC PHAB	D 43	d sec
A	6-11	1922 1927 1929 1945 1953 1954 2012 2014 2017 2019 2034 2036			87.9 96.0 99.5 97.0 97.1 95.9 90.2 92.6 103.8 91.1 99.4 79.9	84.8 91.0 94.3 91.7 92.0 90.9 87.3 88.6 96.9 87.3 93.0 80.4	76.2 83.7 84.1 82.9 82.6 79.0 81.3 91.0 78.6 85.6 71.4	82.6 91.1 91.3 90.7 85.7 88.7 99.6 84.9 975.7 86.0	89.0 97.4 98.3 97.36 97.5 96.5 92.1 105.18 98.2 80.5	90.6 79.9 100.0 99.5 98.7 98.0 92.8 95.7 108.4 92.3 100.7 81.2 92.6	89.6 97.8 100.0 99.8 97.1 93.1 95.6 105.6 98.9 82.1	-2.7 -1.9 -2.5 -2.6 -2.1 -2.6 -3.4 -4.6 -1.3 -1.3	15.0 13.0 10.5 15.0 15.5 14.5 12.5 12.5 17.0 15.5 14.0 21.0

TABLE V (Con't)

06	Sate	Time	A/C	Distance Ft.	EPHL EPHOS	SENEL de	A-level	D-level	*	PHLTH	PRIC	D 49	4
8	5-18	0645	DC-9	2651	87.8	\$1.9	71.4	76.1	81.8	\$2.6	83.0	.2	21.
Ð .	5-18	0743 0743	720	3625	84.3 98.6	\$1.9	71.4	77.0		84.7	64.6	.4	
		97.97	720 726	2416 2663	98.6 86.0	92.5	84.1	92.5 76.8	83.1 96.4	100.9	97.7	-2.3 .8	24. 15.
1			727	2521	89.5	81.3 86.2	70.4 75.6	76.8 8 1.7	82.6 88.4	85.2	84.7		26.
			DO-4	2521 3 8 93	81.0	78.7	6 9 :6	73.7		90.7 81.9	89.6 81.6	-1.2 9	20. 16.
		37			91.0	88.3	76.8	82.6	79.5 89.2	93.6	91.4	-2.6	13. 21.
		0835	1 1		79.1 86.8	78.5 84.6	69.3	73.8 81.3	79.1 87.4	79.7 88.0	80.4 38.7	6	21.
		0851	[27	3052	60.5	80.4	75.9 70.8	74.6	79.6	80.3	62.0	-1.2 .2	18. 21.
		0 8 55 0932	727 727	3135 2274	83.1 88.6	81.8 84.8	72.4	77.2	79.6 83.0	83.7	84.1	6	19.
		1010	580	2821	82.8	81.2	76.5 71.7	83.2 76.0	89.4 82.2	90.4	90.0	-1.8	15. 14.
1		1015	727	3411	76.2	76.1	66.1	70.2	75.6	84.5 76.4	84.1 77.2	-1.7 2	18.
l		1341 1408		-01:	86.1	83.4	73.8	79.5	85.5	86.6	86.5	5	19.
		1412	727 BAC-111	2761 4777	82.5 77.7	81.3 76.9	71.8 66.0	76.5	82.5	83.1	83.6	6	22.
1		1421	DC-8	3852	77.3	77.,	68.7	70.6 72.5	76.4 77.0	76.4 77.8	78.6 78.7	1.3	36. 18.
		1426	VC-10	4587	83.2	83.3	73.6	77.1	82.7	84.5	83.7	-1.3	20.
		1441 1512	BAC-111 707	35£3 1914	76.6 96.6	77.2 96.1	69.5	73.5	78.3	79.0	80.0	-2.4	18.
		1515	720	3182	91.8	85.4	81.7 76.0	91.9 84.3	97.5 89 .6	98.4 94.1	98.5	-1.8	18.
- 1		1526	747	-	90.7	85.4 86.6	75.9	81.5	88.4	91.3	90.9 89.7	-2.3 6	15. 22.
		152 9 1532	DC-8 707	2751	92.2	86.2	75.4	82.9	90.3	93.3	91.2	-1.1	20.
	1	1535	727	2745 2128	92.1 89.6	86.1 87.3	75.3 76.8	82.8 81.4	90.2 87.4	93.2	91.1 89.0	-1.1	20.
		1537	720	277€	90.5	84.5	76.5	84.3	An n	90.0 93.2	90.7	-1.3 -2.7	23. 16.
ı		153 8 1609	727 DC-8	2468	72.5	85.5	76.3	01.6	87 9	88.7	89.2	4	21.
- !		1639	727	3734 2417	£	79.0 82.5	62.3 71.4	72.0 76.2	77.2 82.2	77.9 82.4	79.1	6	26.
ı		1653	BAC-111	2774	65.5	4.55	72.0	75.8	81.7	82.3	83.4 83.6	1.6 1	29. 20.
- 1		1655 1700	BAC-111 720	3308	73.5	74.2	(3.5	€7.2	72.8	74.4	83.6 76.8	9	24.
1		1710	727	2610 2607	85.C 80.0	23.9 13.4	72.3 69.9	76.8 74.1	83.3	84.9	85.4	- 17	30.
- 1		1714	737	2155	€3.5	62.0	71.8	76.8	79.7 82.7	81.5 84.4	81.2 84.2	-1.5 9	16. 22.
- 1		1727 1737	720	2663	3.2	c7.5	78.6	86.6	92.0	96.7	93.2	-3.5	10.
- 1		1823	BAC-111 727	774ء 357	77.Ū	75.0	67.8 69.6	71.6 74.3	77.6	78.7	79.2	- , 3	31.
1		1855	1	33.7	14.5	70.3	62.4	66.7	73.7 71.2	80.2 76.8	81.2 74.8	.7 -7.3	25.1 5.1
'	5-18	1907 1913	707 727	2645 3268	92.6	8:.3	72.å	87 7	91.6	35.2	92.9	-1.0	17.
- 1		1916	707	3063	83.2	7,.2 81.0	70.1 68.6	74.9 73.9	81.3 80.8	02.C 91.9	81.9 82.4	-1.4	20.
ł		1917	727	3268	50.5	79.8	71.4	76.6	83.1	84.6	84.0	1.3 -2.1	27.1 17.
- 1		1920 1936	727	2636	9(.6 93.1	54.3	73.2	79.0	85.6	87.1	87.C	-1.1	18.
1		1938	i	1	3.6	87.1	79.8 79.2	88.3 87.5	92.E 92.B	97.4 97.2	94.0 93.5	-4.3 -3.4	9. 12.
- 1		2005	}	i	£9.5	83.6	72.6	80.5	96.0	90.4	97.0	9	23.
ı		2030 2039	j Ì	ì	87.0 82.0	63.4	70.2	76.6	83.1	85.8	84.7	1.2	37.
ı		2041	1		82.0 85.9	80.6 82.8	68.9 72.1	73.4 78.1	79.1 84.8	79.9 86.3	81.7 86.0	3.1	32.
- 1		2118	! 1		83.0	77.4	(7.9	75.2	81.2	85.5	82.3	4 -7.5	21. 16.
I		2119 2138		[83.0	77.5	69.6	77.4	84.2	84.8	85.3	-1.8	18.
j		2140	[ł	76.6 81.7	75.(79.4	66.0 67.5	70.7	76.2	77.2	76.2	6	26.
1		2141		ļ	88.6	63.5	73.0	73.2 7 9 .1	79.3 86.1	80.3 87.5	80.4 88.1	1.4	30. 22.
- 1		2144		J	92.6	96.3	76.4	84.6	89.5	93.7	91.0	-1.1	17.
']	r-1t	2310	i 1		80.5	78.2	65.4	70.3	76.6	77.9	79.1	.6	45.



TABLE V (Con't)

Pos	Date	Time	A/C	Distance Pt.	EPHL EPHES	ARMEL 48	A-level	D-level	PHILM PHAS	PHLSW PHED	PINC PNAS	D 49	4
В	5-19	07 48 0750	727 727	3625 3742	79.3	78.7 81.5	68.8 71.1	73.4 76.2	78.6 81.9	79.3 82.4	80.2 83.3	.8	24.5 23.0
		0846	bc-8	2869	94.7	88.9	79.1	8 6.9	92.9	96.4	93.9 89.6	-1.7	16.5
		0843	727	2698	59.4	85.5 80.5	75.8	8 2.3	88.5	89.8	89 .6		19.5
I		0907 0915	DC-8	2820 27 8 5	\$1.6 96.8	91.0	72.3 85.4	76.4 93.6	8 2.1 97.7	83.3 101.3	83.4 98.2	-1.7 -4.5	21.5 10.0
Į		0918	DC-8	3046	97.6	90.7	83.5	91.9	96.3	100.9	97.2	-3.3	11.5
i		0928	727	2495 2747	89.3 87.6	85.6 84.0	76.5	83.5	90.2	91. 8 88.6	91.6 88.1	-2.5	14,5 18.5
		095 8 1011	DC-9 727	1966	89.6	86.3	73.9 77.0	80.9 83.5	87.0 90.2	91.5	91.0	-1.0 -1.7	15.0
ì		1049	720	2558	91.2	85.7	76.9	84.0	89.6	93.4	90.9	-2.2	18.0
- 1		1102	720	2776	96.4	90.3	83.3	91.6	95.5	100.2	96.4	-3.8	13.5
1		1128 1402	707	2509 2645	101.0	94.1 89.0	86.6 91.3	95.0 89.3	100.3	103.9 98.2	100.6 95.9	-2.9 -3.4	16.0 11.5
i		1403	BAC-111	2606	79.3	78.0	67.9	73.3	79 4	79.4	81 4	1	22.0
- 1		1411	7.27	2578	86.4	84.3	73.4	78.5	85 1	65.4	86.4	1.0	23.0
!		1450 1501	VC-10 727	3905 2667	94.8 85.4	94.Î 82.4	85.9 73.4	90. 4 79.3	96.4 85.4	96.9 86.2	96.6 86.9	-2. <u>1</u> 9	16.5 26.5
- 1		1505	727	2297	86.3	83.9	75.5	81.1	87.6	98.5	88.3	-2.2	16.5
l		1539	727	2468	85.6	83.6	73.1	78.5 91.8	84.8	85. 5	86.2	.1	20.5
ı		1541 1544	720 DC-8	1800 2611	95.9	90.1 37.2	93.7 76.4	91.8 84.1	95.9 91.1	99.1 94.4	96.5 91.8	-3.2	12.5 28.5
		15**	1 20-0	2011		01.2	70.4	04.1		y4.4	91.0	1	20.9
=]	5-20	2750	720	2510	88.5	84.4	76.4	83.2	88.2	92.6	₽9.€	-4.1	9.5
1		6753	720 707	2663 2910	90.7	86.7 87.0	81.6 79.8	89.3 87.3	92.9	96.0 94.7	93.2 92.5	-5.3 -2.6	9.C
- 1		0755 075 8	727	2667	92.1	91.3	79.3	84.2	91.7 90.5	91.2	93.1	2.3	14.5 37.5
		0802	727	2367	83.3	83.2	73.3	78.3	83.9	85.0	0.39	-1.7	19.C
i		0831	DC-8	2731	\$7.8	85.1	74.5	79.5	85.9	89.1	87.7	-1.3	22.5
1		0834 0836	727 BAC-111	2667 2205	85.7 87.2	84.6 85.7	74.2 76.1	79.1 80.7	85.4 86.5	8 7.2 87.6	86.5 80.2	-1.5 4	17.5 20.0
		0853	727	2053	89.2	8.38	75.9	81.7	88.2	89.3	90.2	1	25.5
- 1		0859	727	2252	89.5	87.5	77.7	82.3	88.6	89.2	90.2	. • 2	32.0
		1202 1434	DC-9	2379 2719	77.9	78.0 93.6	62.6 84.6	72.1 92.5	77.9 98.4	79.4 101.2	79.5 99.2	-1.5 -1.4	17.0 17.0
		1441	VC-10	3010	90.0	89.2	80.4	84.0	90.1	90.1	90.8	1	21.0
		1447	727	2607	77.4	77.4	68.0	71.6	76.8	78.1	78.7	7	19.5
		1454 1457	Bulf II	4102 2924	78.5 91.2	78.2 91.7	71.0 81.2	74.6 85.2	80.2 90.6	80.2 91.3	81.4 91.8	-1.7 1	12.0
		1514	727	3231	87.0	85.1	73.5	78.4	84.5	86.0	86.0	1.5	23.5
		1519	727	2320	83.6	82.5	72.2	77.1	83.3	84.1	25.0	5	2€.0
Ŀ	5-23	1100	720	2610	81.4	80,9	71.6	75.8	81.1	82.0	82.3	6	19.0
•	7-63	1116	720	2837	86.1	81.3	74.7	81.1	86.5	90.8	87.7	-4.7	11.5
1		1130	707	3384	82.2	81.3	71.4	76.2	820	85.4	82.9	-3.2	14.5
- 1		1144 1150	DC-9	3677 3803	79.6	79.9 73.6	70.1 63.3	73.7 67.2	78.6 72.1	79.6 73.1	80.5 73.4	€	23.0 19.0
		1530	DC-8	3440	83.6	81.9	72.7	76.9	82.6	83.2	84.6		26.5
- 1		1555	DC-8	2577	90.4	86.2	76.4	83.1	89.6	92.6	90.5	-2.2	14.5
		1559	727	2900 2774	79.7	79.6	69.8	73.8	79.7	80.6	80.8 87.4	-1.8	22.0
		1626 1820	BAC-111 727	2667	85.1	85.3 82.1	76.7 71.6	80.3 75.9	85.7 81.8	86.9 83.6	83.3	9	20.6 18.6
	5-23	1901	707	3233	84.8	83.0	73.1	78.1	84.4	88.3	86.2	-3.5	14.5
٠.	,-,-,	1916	727	2000	88.5	86.9	78.0	82.8	88.8	89.7	89.7	-1.2	17.5
1		1918	727	2000	86.1	84.€	74.4	79.1	85.4	86.3	86.8	-0.1	22.0
- 1		2015 2033	1	\	83.1	85.0 81.7	75.7 72. 8	78.8 76.5	83.4 82.2	84.3 82.9	84.0 83.1	-1.2 -1.4	19.5 19.5
		2126		1	77.4	79.0	68.1	71.8	77.2	78.8	80.1	-1.4	18.0
		2147		1	93.5	87.8	78.8	86.3	92.3	97.1	93.1	-3.6	9.5
Ł	5-23	2215		1	84.2	83.9	75.5	79.5	85.3	85.8	85.9	-1.6	17.
		2302	I	l	88.5	83.5	75.1	82.7	87.8	92.3	88.9	-3.8	12,5

TABLE V (Con't)

Peo	Date	Time	A/C	Distance Ft.	ETIL. ETIL	2010Z. 49	A-level	9-level	PREAL PROB	PHILIPA PHAR	PHLC PHOS	D 48	4
•	5-24	1439 1444 1453 1501 1513 1516 1640 1645 1647 1702 1703 1705 1708 1720 1723 1730 1730	727 727 727 727 747 720 DC-8 BAC-111 707 DC-9 BAC-111 727 727 727 727 727 727 727 727	1903 2274 2168 2627 2610 2610 1911 2020 2385 2651 2389 2495 2864 2771 3440 2442	90.5 90.7 96.7 97.0 94.4 97.0 101.7 86.8 87.3 99.5 84.1 97.3 78.2 88.9	86.2 86.6 83.9 90.5 89.8 97.1 82.4 94.7 84.3 92.1 81.7 90.0 78.5	76.5 78.0 74.7 85.1 79.5 81.8 86.5 71.5 73.7 78.0 84.5 71.5 70.9 83.4 72.9	83.2 85.2 80.3 89.5 90.3 94.6 76.6 91.4 93.1 76.0 92.8 81.4	89.9 91.5 85.7 91.7 91.7 94.8 101.2 86.8 88.4 88.0 98.1 83.7 96.7 81.7 85.7 85.7	91.6 92.3 87.7 93.9 99.9 104.1 83.6 105.4 87.4 88.9 102.9 84.7 101.4 84.7	90.7 92.4 97.5 97.5 93.0 96.3 101.6 80.4 88.6 98.8 85.2 97.6 85.2	-1.6 -3.3 -2.9 -3.7 -3.7 -1.6 -3.8 -4.9 -1.8	19.5 18.0 19.0 27.0 29.0 14.0 30.0 11.5 22.0 19.0 10.00 10.00 11.5
2	5-25 5-25	0900 0903 0907 0911 0919 1054 1102 1103 11714 1716 1800 1822 1903 1907	HS-125 580 737 720 BAC-111 720 737 DC-9 727 DC-9 BAC-111 727 727 727 727 727 727 727	2917 2194 2262 2039 2867 4410 2610 2623 2133 2486 2231 1614 2774 2698 2719 1487 2262 3588 3144 3178	87.7 75.4 98.8 79.5 86.2 79.5 87.8 98.2 92.3 87.6 89.4 97.1 83.1	87.1 83.2 76.2 93.1 84.8 79.6 79.5 84.3 92.2 89.1 86.8 91.0 81.7 89.5 89.9	77.8 72.7 67.2 64.7 74.0 68.9 73.9 74.3 77.3 81.9 77.3 81.1 81.1 81.1 81.1 81.1	81.58 73.193.44 73.3.26 81.193.44 88.198.78 891.27 88.4 891.20	87.8 82.0 79.2 85.76 87.5 87.5 78.8 96.7 91.6 87.5 91.6 87.5 94.5 94.5 96.1	85.1 79.0 101.7 85.3 83.7 790.1 100.9 93.0 93.0 98.5 997.9 98.3 98.3 98.6	88.8 81.400 87.9 87.9 87.9 97.9 98.3 95.9 95.9 95.9 95.9	6 1 -3.6 -2.2 .5 1.2 7 -2.3 -2.7 7 -1.9 -1.6 -1.7 -2.1 -1.8 -2.7 -4.6	23.5 20.5 12.0 16.5 29.5 26.0 96.0 12.5 20.5 21.0 13.5 12.5 12.5 12.5 24.5
		1910 1912 1916 1922 1923 1925 1927 1930 2143 2149	727 DC-9 727	3028 3028 1870	88.6 96.8 96.7 83.7 96.9 82.3 87.4 80.9	87.2 93.7 90.7 82.6 90.1 81.7 85.2 79.7	71.0 76.3 83.7 81.3 73.1 82.1 71.8 75.6 72.6 68.5	75.0 80.8 88.7 88.9 77.3 90.3 75.9 81.4 77.1	87.0 95.0 95.1 82.8 95.3 81.7 87.4	80.6 88.7 98.0 83.3 99.9 82.8 88.6 83.1 77.9	88.5 96.4 96.1 84.3 96.2 83.0 89.2 78.0	-1.3 -1.3 -4 -3.0 5 -1.2 -2.2	36.0 25.5 17.5 27.0 12.0 22.0 16.0 12.5 21.0

Pee	Date	Time	4/0	Materia		T	A-level	3-level	Z.	武	H	•	9
c	5-18	0645	25-9	3364	79.0	78.4	67.0	73.4	70.6	19.7	79.7	-0.7	24.5
C	5-18	0742	720 720	33775		II:I	vii	R:S	1	\$0.2 \$0.3	19:0		#:
		0000	726	522	1	<u>B</u> ∙3	15.8 70.0	70.5 76.0	7.3		73.0	4:3	23
		***	137	95			67 - 2	71.9	11.5	77.7	12:	1:3	
		0749 0000 0004 0009 0021 0625	20-8 197		73.7	71.2	67.2 74.8 63.8 69.6 68.7	13:	73.3	75.		-3.3	16.6
		0034 0051	127 127	4519 3643	78:3	₩:}	3 .7	73.3	73:3	75.0	79.2	-1.5	30.0 34.0
		0807	8-90		72.4 06.0	11.0	90.5	97:7 77:7	72.7		173.1	-1.7 -0.3	14.0 21.5
		0909 0932 1010	720 727 5 86 727	2559 2652 2963 4484	82.3 76.7	86.5 78.3	70.1	75.1	H.		38.1	-0.3	34.5 36.0 36.5
[1014 1052	THE I	1111	1 79.A	13.6	Q: 6	72.7 64.9	13-3	73:7	14-3	-Ī. į	36.5 32.0
		1103	737 7 30	2919 3309 3094	1 37:3	73.5 76.3 87.3	70.1 60.7 61.6 65.6 74.1 61.2	70.2 91.6	77.7	21-2	76.3 76.3 92.7	4.1	12.5
	1	1114	720 DC-8	2794	76.7 87.6 94.8 52.8	61.	72.5	01.6 09.5 76.0	R :7	F :3	B :	4:1	18.0
		1133 1153	727	2818	\$3.3 \$3.7	19:7	71.3	78.6 75.8	23:1		55.1 53.2 53.1 53.1 63.5 64.5		13.0 24.5
	l	1210	Jot Com 727	2636 3188 3164	13.7	70.1	70.3 70.5	75.4 75.4	61.0 61.4 76.2 74.7	62.4	23:2	-3.7 -4.3 -4.5	19.5 24.5 6.5
	1	1250 1338 1406	100.0	2531 2532	92.2 72.8 92.1	68.2	64.2	13.3	75.3	12:3	61.5 02.9	-4.5 -4.3	6.5
	1	1270	727 MC-111	4607 6992	73.2	72:5	70.0 63.2	73.8 75.1 69.9 79.7 76.7	73.7	73.3	ij.i	-2.0	13.0
		1452 1448	VC-10	6992 1561	74.9	76.8 77.7	\$1.2 \$6.0 70.7 77.5	79.7 76.7	13.2 67.8	75.2 76.1 84.5 97.9	64.4 69.3	-1.2 -4.0	19.5 9.5 34.0
İ	ļ	1511 1514	10-26 10-8 720	1 2226	90.0	77.7 89.4 82.5	77.5 75.3	رَ رو و.را	87.5	87.9 82.1	99.3 99.2	2.1 -4.3	12.0
1		1531	DC-8	3858 3004 2684	80.2	87.0	77.0	41.2	97.5	#: 1	89.2 67.9	-4.3 0.6 1.5	26.0 26.0
1	1	153 4 15 35	727 720	3107	W.1	87.8 83.3	76.5 73.6	81. 8 80. 8	87 . 7 86 . 6 83 . 5 75 . 6	5.3	7:1	-1.1	19.5
ł		1537 1608	727 DC-8	2900 4097	13.6	81.7 76.2	72.4 65.9	77.6 69.9 62.4	75.1	89.9 85.6 76.0	95.6 76.5 84.2	-1.8 0.6	17.0 20.5
l		1612 1628	707 BAC-111	3118 3308	88.5 17.7	\$3.2 77.9	65.9 73.3 68.6	62.4 72.5	97.6 76.1	99. 7	81.4	-1.6 0.3	15.5 24.5 29.5
Į.	1	1636 1645	727 Oulf I	3045 2917	82.9 78.7	81.5 78.0	73.4	72.5 75.9 72.3 76.3 69.5	76.1 61.5	41.7	83.6	1.: 0.1	30 -0
1	l	1651	BAC-111	1000	1 12.0	82.6	12:3	ŢĞ.Ş	77.9 80.0 74.0	92.9 773.8	19.6	0.1	81.0 84.5 24.0
1		1651 1658 1659	PAC-111 720	3583 2757 2761	3:5	75.2 03.2	79.3	77.0	62.0	35. 6	43.4	1.3	29.6
	1	1709 1712	727 727	3107	75.8 83.9 77.1 81.9	76.2 80.9 70.8	79.9	72.2 74.2	79.8	90.4 83.2	79.5 83.6 76.4 76.4	-3:3	3.
	ļ	1735 1860	580 727	4232 3445	69.7 79.6	70.8 78.5	61.5 68.1	65.3 72.7	78.0 79.8 68.2	71.1	72:3	-1.4 0.3	33.5 23.5 25.0
c	5-18	1906	707	2949	93.1	87.0	77.6	05.6	90.1 90.0			-1.2	18.5
		1915 1917	DC-8 727	3624 3587 3163	1 02.5	79.5 79.7 82.8	67.9 70.6	99.6 73.7	81.7	24.3 53.7	2.4	0.5	29.5 13.0 26.5
	ļ	1919 1921	727 DC-8	3163 2772	85.6 86.9	82.8 82.4	71.9	77.3	84.0 84.2	7:3	33:3	0.3 -0.5	20.5 12.5
	1	19 36 19 38	720 707	2575	92.7	86.8 82.8	77.8 74.2	\$6.0 \$1.2	91.3 67.3 90.4 93.4		95.2 95.4 97.6	-3.0 -2.1	12.5 13.0
	1	2004	'"'		92.2	86.4	78.0	84.2	\$2.£	90.3 94.1 13.7 63.0 84.0	91.9 91.9 82.9	7:3	13.0 15.0 27.5
1	1	2005 2028	ł	1	75.8	70.9	71.3	74:\$	13: 1	18: 7	M:I	0.1	27.5
	1	2037 2039	1	1	84.7	81.1 82.2	69.6 71.7 64.2	74.4 77.3 10.2	\$0.5 \$3.7 76.3	# :§	1	-0.1	27.5 25.5 14.5
		2117 2136			78.1	73.8 79.2	60.7	85.0	70.9	79.9	78.4	-2.5 -3.8	8.0
1		2137 2138	1	1	79.9 82.5 76.6	77.9 80.1	67.0 70.8	72.5 75.9	11:1	70.9 76.5 83.1 76.3	.	-6.6	28.5 24.5
1	1	2156		1	1	75.8	65.1	69.1	75.2		76.3	0.3	25.0
1		230\$			78.0	77.3	65.4	69.4	75.2	76.2	77.5	1.0	27.0

TABLE Y (Lon't)

The transfer of the second second second second second second second second second second second second second

		· · · · · · · · · · · · · · · · · · ·	A/C	Distance Ft.	EPIL EPINS	49	A-lovel	D-level	PHO	PLAN ECH	PMC	D 48	d .
C	5-19	0 958 1010	DC~9 727	3109 24 8 5	86.0	\$2.8	74.0	80.4	96.7	\$7.8	87.1	-1.8	18.5
1		1048	720	2836	86.5 89.8	#3.3 #4.6	74.8	80.8 83.6	87.0 88.8	\$8.6	87.8	-2.1	15.5 11.5
	•	1053	737	3016	87.4	85.5	76.5 75.7	81.6	77.6	92.5 99.2	89.7 88.6	-2.7 -1.8	18.0
	·	1182 1185	720 727	305 8 2676	95.7 83.4	89.1 81.4	U 2.1	90.5	44.7	99.7 84.2	95.8 84.1	-4.0	11.5
- 1		112,	707	2645	100.3		71.2. 84.4	76.7 92.9	82.9	34.2	84.1	-0.5	19.0
- 1		1217	DC-9	2209	87.2	93.1 83.8	75.2	ง กั.กุ	97.9 87.6	102.5	99.2 88.5	-2.2 -1.2	15.5 14.5
		121 8 1220	727 DC-9	4046 2840	72.9 82.8	72.1	65.2	70.8	70.4	76.4	78.2	-3.5	11.0
		1222	DC-9	2676	82.1	81.8 80.3	71.3 70.7	76.0 75.9	81.7 81.8	8 2.5 8 3.6	83.0	0.3	24.0
1		1226	Oulf II	1649	72.2	73.6	67.2	71.0	75.7	76.2	83.4 76.3	-1.5 -4.0	17.0 10.5
- 1		1239 1248	lear 727	3411	71.9 80.4	73.5	67.4	71.1	75.7	76.2	76.7	-4.3	10.5
- 1		1306	580	2674	76.3	80.2 75.1	70.2 64.9	74.7 69.8	80.5	81.8	\$2.8	-1.4	16.5
ŀ		1344	DC-9	3257	87.6	84.6	76.0	81.6	75.8 87.8	77.7 89.8	78.4 89.2	-1.4 -2.2	16.5 14.5
1		1402 : 404	707 BAC-111	2730	94.2	88.7	81.9	89.8	94.1	98.2	95.8	-4.0	9.5
ŀ		1446	Jet-Star	3258	76.5 84.8	76.3 84.5	67.1	71.7	77.5	77.5	79.1	-1.0	18.5
- 1		1450	VC-10	2580	93.7	92.5	75.5 82.7	79.9 87.3	85.4 93.4	86.0 94.0	86.0 95.3	-1.2 -0.3	19.0
		1505	127	2521	84.3	82.7	79.0	78.8	84.7	85.2	85.5	-0.9	22.5 17.5
i		153 8 1540	727 720	2829 1864	83.0 93.8	81.2 88.0	73.3	78.2	84.8	85.7	85.4	-2.7	17.5
ŀ		1543	ĎC-8	3510	92.7	86.6	"1.5 .0	88.9 84.3	. 94.0 90.7	97.5 93.2	94.5 91.3	-3.7 -0.5	9.0 21.0
C	5-20	0644	DC-9	4171	79.0	78.8	ć7.5	72.0	77.4	78.4	79.9	0.6	26.0
C	5-20	0750	720	2816	88.9	84.5	75.i	82.7	87.7	92.3	89.0	-3.4	13.5
1		0753 0755	720 707	2878 3969	92.0	87.3	80.7	88.0	92.3	95.4	93.0	-3.4	11.5
ļ		0757	727	2024	90.0 91.5	84.7 89.4	75.5 79.4	82.7 83.9	87.5 90.0	91.8	39.6	-1.8	14.5
j		0801	727	56.66	83.4	82.4	76.8	75.6	81.3	91.1 82.7	91.7 83.1	0.\$ 0.7	26.5 28.5
- 1		0831 0833	DC-8 727	301f 287f	E9.2	86.0	76.2	81.C	87.6	90.5	88.9	-1.4	22.5
- 1		0835	BAC-111	2388	80.4 83.2	81.0 82.3	70.3 73.1	74.4 77.2	79.4 82.1	79.9	81.9	0.5	23.0
		0853	727	2274	85.0	83.5	74.0	73.1	84.8	83.4 85.5	84.9 86.7	-0.2 -0.5	21.0 22.5
- 1		0858 0917	727 BAC~111	2075	89.3	87.4	77.5	82.1	87.6	PS. 7	39.3	0.6	26.5
- 1		0944	727	2507	81.9 83.4	81.5 82.9	70.3 72.2	74.5	80.2	01.4	62.2	0.5	25.5
- 1		1103	720	2778	88.0	84.2	76.1	76.5 83.1	81.9 87.9	82.5 92.5	83.3 89.9	0.9 -4.5	25.5 9.0
- 1		1126 1128	720	2757	31.3	86.9	78.2	85.7	90.ó	93.6	91.2	-2.3	16.0
- 1		1120	707 DC-9	2711 32 ⁹⁸	93.0 77.4	87.9	79.4	87.0	90.€	93.7	92.5	-0.7	17.5
- 1		1254	727	2485	82 2	77.3 61.0	68.1 69.1	72.9 73.5	78.3 79.4	79.3 79.4	80.0 81.0	-1.9 2.8	14.0
1		1343	DC-9	3352	84.2	82.0	71.0	73.5 76.6	82.8	84.0	84.2	0.2	31.0 27.0
l		1414	BAC-111 727	3742	82.1 80.8	81.6 80.0	73.4	<u> </u>	03.2 70.2	83.8	84.7	-1.7	19.0
i		1417	DC-9	3051	85.0	83.1	67.7 71.4	72.4 76.5	70.2 82.3	79.1 83.7	80.4 84.6	1.7	35.0
- 1		1432	707	"97]	85.0 98.8	92.8	82.6	90.5	96.7	99.6	97.5	1.3 -0.8	32.5 19.0
c	5-23	1143 1533	DC-9 DC-8	4023 3853	80.5 81.4	80.2	68.7	73.2	78.4	79.6	80.3	0.9	33.5
- 1		1546	VC-10	3052	85.6	81.5 86.0	74.0 75.5	78.4 79.3	83.8 84.4	83.8 84.4	84.4	-2.4	18.0
1		1601	727	3000	77.2	78.1	67.5	71.4	76.6	77.5	85.8 78.9	1.2 -0.3	27.5
- 1		1603 1024	737	2051	75.1	75.6	65.5	70.2	75.5	76.4	76.6	-1.3	19.5
c	5-23	1905	7 17	3068	80.3 82.6	80.3 80.6	70.0	74.4	79.6	80.3	80.5	Ō	55.0
ļ		1907	'''	1	93.2	88.7	71.1 79.4	76.3 84.8	8 2.2 91.5	85.9 94.5	83.2 92.6	-3.3 -1.3	13.0
		1911	1	1	78.0	77.8	66.3	70.5	76.1	76.8	77.2	-1.3	42.2
ſ		1918	1	ĺ	82.9 85.9	82.3	72.8	77.4	\$3.3 \$4.0	84.2	83.9	-1.3	18.5
		1929	1	1	83 0	84.7 70.8	76.3 68.7	80.5 75.1	81.4	96.8 96.6	86.9	-0.9	17.0
- 1		1950	l	I	83 9 77.8	77.3	65.0	69.8	75.9	78.6	83.1 77.2	-2.7 -0.8	11.0 27.0
		2036	!]	80.9	81.6	73.4	76.7	81.4	82.3	82.5	-1.4	14.0
1		2130	[1	81.3 78.9	81.6 79.6	71.6	75.4	80.G	81.5 79.6	81.5	-0.2	21.5
		2152		į.	92.1	86.0	70.1 76.6	73.8 84.5	79.0 8 9 .9	79.6 95.6	80.4 91.3	-0.7 -3.5	22.0 8.5

TABLE V (Con't)

Pos	Date	Time	A/C	Distance Pt.	rpal Epale	SENEL.	A-level dBA	D-level dBD	PREA PRAB	PALTA PALTA	PREC PRO	D es	4
С	5-23	2218 2306			\$3.6 \$6.8	82.7 82.4	72.8 73.6	76.8 81.1	82.5 85.3	83.3 86 ,	84.0 86.5	0.3 -1.7	21.0 17.5
С	5-24	1322 1343 1345 1345 1400 1415 1427 1434 1500 1515 1517 1522 1539	DC-9 707 DC-9 BC-9 BC-111 707 DC-9 707 727 VC-10 747 720 707 720 727 Gulf II DC-E 727	2973 2910 3386 2530 3440 3257 2859 2851 2859 2851 2576 2576 2576 2576 2576 2576 2576 2576	99.7 82.3 85.5 78.1 95.5 78.1 90.6 91.1 97.5 97.5 97.5 92.4 92.4 75.6	78.7 792.5 80.3 80.3 80.3 80.3 80.3 80.3 80.3 80.3	69.0 69.6 74.0.7 66.6 60.2 66.5 76.4 85.7 85.7 85.7 85.7 85.7 85.7 85.8 86.5 87.7 85.8 86.5 86.5 86.5 86.5 86.5 86.5 86.5	74.2 78.3 78.3 78.3 79.3 85.3 85.3 85.3 85.3 85.3 85.3 85.3 85	81.0 87.3 85.3 77.4 91.0 97.4 90.2 91.5 96.4 93.2 96.4 91.6 82.9 96.4	82.7 101.1 85.35 78.38 78.38 79.27 92.75 97.77 94.59 103.8 92.4 93.4 93.4 93.5 93.5 95.0	91.8 98.0 85.8 97.6 94.7 79.0 90.7 98.0 98.0 98.3 98.3 98.3 98.3 97.5	-1.8 -3.0 -2.8 -1.4 -2.8 -1.6 -1.6 -0.2 -3.3 -0.6 -0.5 -0.6 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5	19.0 17.0 19.0 26.5 30.5 15.0 23.0 21.0 15.5 26.0 18.5 9.5 19.5 22.0 18.5 17.0
С	5-25	062¤ 0649	727 DC-9	2974 349.	80.3 84.4	79.8 52.6	6 8.7 72.5	73.6 77.1	79.2 83.0	79.8 83.8	80.3 84.7	0.5	25.0 29.0
С	5-25	0708 0754 0800 0802 0805 0808 1101 1101 1111 1120 1201 1328 1345 1801	DC-9 720 727 DC-8 707 707 DC-9 720 727 DC-9 737 720 LC-9 HC-125 707 DC-9	.351 3132 3050 3050 3089 2852 2651 2776 2540 2442 2515 3235 4329	89.86 897.83 97.45 97.75 99.54 99.54 64.83 169.67 98.7	85.1.4 91.4.2 92.8.0 91.9.3 87.4.9 87.4.9 87.4.8 83.9.4.9 83.9.4.9 83.9.4.9	76.1 83.7 72.5 93.9 83.9 83.9 72.6 87.3 72.2 83.8 77.3 83.8 77.3 83.8	82.5 76.9 85.0 87.8 91.7 76.6 91.9 82.6 79.6 79.6 79.6	896.913.639.264.3651 896.99.364.3651 896.99.364.3651	90.4 101.3 83.9 93.6 98.6 98.6 31.3 101.3 90.5 90.6 97.7 77.0 101.4 89.3	89.1840188768993.89998897789998897788.206	-0.6 -3.7 -0.5 0.2 -2.1 -0.9 -3.8 -3.3 0 -2.6 -1.9 -9.6 -1.1 -0.9	21.0 10.5 22.5 23.5 17.5 25.0 9.0 11.0 23.5 16.5 23.0 16.5 17.0 19.5
С	5-25	1906 1910 1915 1924 2004 2149 2150			84.0 90.2 91.8 81.3 77.2 77.1 93.7	83.3 68.0 87.4 80.2 77.7 77.2 88.1	73.4 78.1 77.7 71.5 66.2 70.5 79.4	78.0 83.2 84.2 76.7 70.4 73.5 87.6	83.7 89.0 30.1 82.2 75.8 79.0	84.9 97.0 93.2 82.7 76.8 80.4 96.7	86.3 91.6 91.8 83.5 77.9 79.4 93.4	-0.9 0.2 -1.4 -0.4 0.4 -3.3 -3.0	21.5 25.0 20.5 18.0 30.0 15.5 14.5

TABLE V (Con't)

Pos	Date	7100	A/C	Distance Pt.	EFFE.	SENCE.	A-level	S-level	PINEA	PRESE	PHLC	D	d
D	6-3	1648 1698 1754 1808 1844	727 727 737 727	3135 3412 4022 3569	10:1 17:3 15:8 19:2	87.2 83.6 76.0 83.3 89.2	70.2 72.1 67.4 72.6 60.9	83.9 77.5 78.4 77.9 84.7	99.8 93.8 78.2 94.9 69.9	91.0 85.8 79.6 86.4 90.6	91.7 85.5 79.4 86.3 90.8	3 -2.1 0 -1.4	23.5 27.5 14.0 20.5
D	6-3	1424 1435 1456 1506 1508 1540 1651 1602 1636 1636 1715 1712 1712 1812 1812 1825	DC-9 BC-8 727 707 720 720 727 737 BAC-111 727 727 727 727 727 727 707 707 707 707	3931 4061 4070 4099 4078 3855 3824 3620 4778 4640 4549 3909 3625 4000 4217 3854 4218 3515	84.7 91.7 82.05 82.05 82.05 82.05 82.05 77.3 72.2 77.7 77.7 77.7 83.7 83.7 83.7 83.7 83.7	845.64.158.158.158.158.7558.24.598.7558.24.598.7558.77788.77788.77788.77788.77788.77788.77788.77788.77788.77788.77788.77788.7788.77788.77788.77788.77788.77788.77788.77788.77788.77788.77788.77888.7788.7788.77888.77888.7788.7788.7788.77888.77888.77888.77888.7788.7788.7788.77888.7788	73.34 76.59 770.59 77.45 66.42 66.46 64.7 66.3	79.98 75.165.35.93.765.35.165.35.370.39.566.265.35.39.566.265.35.39.566.265.35.39.566.	85.2 85.1 86.0 86.0 91.0 75.9 75.9 75.1 75.2 94.3 77.0	86.7 92.3 83.0 98.8 98.8 98.8 98.7 98.7 97.7 97.9 98.5 99.5 99.5	86.2 91.3 87.5 82.7 77.9 76.6 75.9 76.5 77.4 895.0 77.6	-1.8 -1.29 -3.63 -1.8 -1.7 -1.7 -1.9 -1.9 -1.9 -1.9 -1.7 -2.6	24.5 19.5 19.0 21.5 19.5 18.0 20.0 28.5 22.5 31.0 22.5 11.5 11.5
ن	€-3	1919 1956 2106 2110 2147 2215 2300	720 727	4500 3742	88.9 22.0 78.6 69.2 87.2 67.2	83.7 80.7 77.5 71.3 81.6 70.7	73.5 69.4 64.7 62.6 72.5 60.5	80.8 74.1 69.8 66.7 80.1 64.3 73.9	80.2 85.4 80.2 75.1 70.5 83.6 67.2 79.8	81.2 89.5 80.8 76.7 71.5 87.6 67.7 30.3	82.5 87.7 80.9 76.8 71.3 85.1 69.4	2.2 6 1.2 1.9 -2.3 4 5	40.0 19.5 29.5 34.5 22.5 20.5
L	6-4	0756 0801 0801 0812 0812 0832 0852 0852 0857 1533 1533 1545	727 737 720 DC-8 DC-8 727 DC-9 BAC-111 737 727 747 720 DC-8 727 720	4296 4763 4078 4469 3742 3625 5649 3771 34123 3896 47164 4424	875-14918336141 975-14918336141 10000000000000000000000000000000000	81.55 81.55 81.59 81.61 81.61 81.61 81.61 81.61 81.61 81.61	69.8 74.2 72.2 69.8 67.1 68.6 68.6 74.5 71.9 70.4	70 -9 -1 -5 -2 -8 -6 -5 -2 -8 -2 -7 -7 -5 -2 -8 -2 -7 -7 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	792.35 792.35 793.53 778.77 776.5 7776.6 880.6 881.9	63.50 63.50 90.48 80.32 71.26 80.32 71.26 88.9 93.12 88.9	878677788.339.3563623	1.7 2.2 -2.5 -1.7 1.6 1.9 -1.9 -1.7 1.0 -1.6 -3.5	30.0 16.0 19.0 31.5 40.0 16.0 35.0 27.5 32.0 11.0 36.5
٥	Ģ-4	1904 1911	727 DC-9	3362 5429	72.5 74.4	71.5 74.9	59.8 62.1	66.4 66.8	72.1 72.0	02.5 72.7 73.0	90.0 75.3 74.2	-1.4 2 1.4	18.5 21.0 36.5
į.	(-5	1059 1103 1106 1113 1115 1119 1338 1418 1524 1719	737 DC-8 DC-9 727 720 DC-8 DC-9 727 727 727 707	4209 4410 3569 4462 4078 4430 4471 3932 4296 2598	77.4 90.7 85.4 81.1 74.2 79.6 82.4 82.2 94.3	7:.5 8:.2 8:.1 79:9 72:6 78:5 80:0 80:8 80:8 89:0 81:3	68.1 74.9 71.2 69.8 63.4 67.0 68.9 70.4 69.6 81.7 74.3	71.4 83.0 78.3 74.8 69.7 72.2 74.1 75.5 75.1 89.9 81.8	77.8 R9.0 84.8 80.6 75.3 76.7 79.5 81.0 94.0 86.1	81.3 92.8 86.8 81.5 81.5 81.3 81.3 61.3 61.7 61.7	80.1 90.6 86.2 81.8 77.6 81.7 82.55 95.6	-3.1 -1.2 -3.6 -1.3 -3.6 -1.3 -3.7	21.0 19.0 26.0 26.5 27.0 21.0 9.0

MALE V (State)

200	2000	T)eo	4/0	Photomos	3		A-Jaros	8-level	POLA POLA	PRESIDE	PHLC	1	-
°	6-5	21.06 21.36 21.46			18:5 53:0	#: : 6:3	12:3 73:3	\$7.2 \$1.6 \$0.5	11:1 17:1	22:3	#:} #:;	-2.1 -3.5	27.5 28.5 28.5
D	6-6	0049 0051 0950 1033 1039 1054 1056 1057 1109 1111 1126	200-111 727 726 20-9 727 20-9 707 720 737 720 50-6	15 25 25 25 25 25 25 25 25 25 25 25 25 25	00.2 74.1 83.2 81.4 79.9 92.8 86.0 77.9 86.4 86.3	70.1 74.8 79.5 80.9 80.0 77.7 86.4 81.1 76.4 80.9 82.4	\$7.1 61.7 70.3 71.0 70.8 70.0 77.6 72.6 66.1 73.7 72.4	61.4 66.6 77.3 77.1 75.7 75.7 75.9 79.9 71.5 60.5	66.0 71.3 82.6 81.5 81.3 91.2 84.5 76.8 85.5	67.4 71.8 95.2 85.4 82.6 95.6 88.1 77.8 89.3 90.5	71.9 74.3 83.9 84.8 82.2 81.8 92.9 78.9 86.9	.8 2.3 -2.0 -1.6 -2.7 -2.8 -2.1 -2.9 -2.2	29.0 40.5 17.5 15.5 15.0 14.5 16.0 25.5 17.5 17.5
D	6-6	2019 2059 2115 2119 2122 2126 2129 2139 2141 2152			80.2 79.6 86.2 86.8 77.7 84.5 99.4 93.2 76.7 91.3	82.8 78.8 79.5 81.0 76.2 81.6 83.0 79.6 76.0	74.6 69.0 74.2 69.4 65.7 71.0 72.5 67.0 63.3 67.6	61.8 73.7 82.8 77.3 72.6 76.9 80.1 72.6 68.4 73.4	88.0 79.5 86.3 83.7 78.8 83.5 86.1 78.5 79.6	93.7 92.2 80.4 91.9 87.9 82.0 85.3 90.2 81.7 780.5	84.3 89.1 80.9 88.7 86.1 80.7 84.4 87.9 82.1 77.8	5 -4.0 -5.7 -1.1 -3.8 8 1.5	6.0 20.0 6.0 21.0 11.0 29.0 23.0 33.5
b	6-7	2202 0800 0801 0803 0806 0822 0831 0833 0834 0837 0844 0855 0855 0856 0956	727 720 727 707 707 727 720 BC-8 727 727 500 737 737 727 727 727	4000 4745 4296 4099 5118 4673 4673 46218 4778 3362 3362 3620 5273 4076 4796	73.9 83.0 87.1 88.7 98.5 78.4 79.6 82.2 77.4 63.6	81.5 81.1 61.1 79.6 84.4 83.8 81.5 76.2 80.9 76.9 81.0 80.5 77.7 81.2	70.9 68.9 71.4 67.3 73.6 74.3 68.4 70.9 69.2 72.4 67.2 79.4	74.9 74.9 79.7 73.0 82.7 73.4 75.1 73.8 72.8 72.9 76.1 71.9	79.7 80.9 84.6 79.4 87.1 79.3 82.7 79.6 91.0 77.2	79.7 82.2 89.3 81.0 92.6 81.0 83.3 79.1 88.3 78.6 77.2	82.1 82.9 85.7 80.8 81.9 81.8 84.0 81.8 82.7 78.4 83.2 78.2	.8 +0.8 +2.8 -1.3 -1.3 -2.2 -1.6 -1.6 -0.6 -0.1 -0.2	27.5 6.5 28.0 12.0 24.5 21.0 15.5 18.5 18.5 19.5 27.0 31.5 19.5 18.5 18.5 24.5

MALE V (Oun't)

Poe	Date	Time	4/6	Matemee Pt		-	A-Jovel	3-350-1	75	Times Times	74	-	-
D	6-7	1042 1045	M9-133	1000	80.7	79.3	4.10	73.4	79.1	50.6	A 0.5	.1	85.0
1		1046	107	8653 9932 6333	17:1	79.3 70.0 62.6 85.1	9 .:	B:i	3: t	¥.;	E :	-1.9	21.0
		1106	100-8	iii i	81.5	5.1	25.0	Ľ:I	2:3	27.7	7.4	-1.6	17.5
		1115	727		94.6	12:2	49. 6	79.9	80.5	11.5 10.5	11. 3	- :}	27.5
		1120	707			63.2	70.0 74.9	70.0 64.0	91.2	95.0	27.5	-1.9	35.0
		1191	727	2024	20:0 12:0 14:3	11.2	70.3 70.3	7:3	7.4	91.1 9:1 W.1	81.5 99.5 80.7	-1.4	18.0 19.0
		1154	DC-9	R.E.	63.3	\$0.8 \$1.4	70.5		20.5	M. i	83.9 93.5	.ž	22.0
		1154 1156 1226	727	1000	81.0	79.8	71.3	71: \$	23:1	#:;	23.3 62.3	-1.1 9	23.0 27.5
1		1237	BAC-111	5931	80.6 74.5	78.6	69.5 65.7	74.8	39. 7	81.7	i.i	-1.1	4.3
- 1		1254	727	3625	62.2	74.6 80.7	95.7 72.1	69.3	74.0	75.6	77.2	-1.3	23.0
1		1254 1312 1324	500	3991 4145	10.5	79.1	71.6	77.0 73.6	12.9 13.1	, te.9	83.4 81.8	-2:7	23.5
		1320	DC-9 DC-9	4471	78.9 76.2	77.6 74.9	51.4	72.7	78.5	79.Z	79.3	3	ää
		1320 1342	DC-9	3353 3625	66.6	8 3.2	68.2 74.7	72.9 60.7	79.0	R:2	79.3	-3.7	10.0
		1345 1409	727 727	3625 4143	£1.2	70.8	64.3	73.6	79.2	80.1	82.3	-1.8 1.1	17.0
i		1419 1421 1422 1424	737	3771 i	81.2 81.1	80.3 70.3 76.7	71. š	76.1 72.9	£2.4	83.2 80.2	23.3	-2.0	. 17.5
		1421	727	1070	79.7	76.7	71.7 70.4	17:2	79.2 63.4	7.3	#.5	-5.i	. .
- 1		1424	DC-9 DC-8	41.45 37.95	10.7	78.8 83.9	70.4 74.0	13:7	81.7 86.7	82.4 86.4	81.9 87.3	-3.7	7.5
- 1		1433	DC-9	3735 4560	70.2	77.3	60.1	77:1	2.7	79.4	97.3	6	32.0
		1437	DC-8	4067 4207	91.2 90.0	95.3 80.8	75.0	72.4	M.,	91.5	13:1	-1.2	33.5
- 1		1442	DC-9	4385	11:j	79.6	79.8 64.9	74.9 74.2	80.2 80.5 84.6	80.5 81.6	5 1.6	5	23.5
- 1		1506 1508	727 727	4000 4000	\$2.5	79.9	13:3	79.0 75.0	#:3	85.9	11.2	.ì -3.1	29.5 13.5
- 1		1509	580 I	3511	83.7 70.8	60.9 75.1	2.	75.0	82.5	95.9 94.1	22.9	4	23.0
ł		1515	7-39	3800	78.3	79.1	65.3 70.4	71.3 72.2	76.0 77.2	78.2 77.8	78.7 79.5	-7.4 .5	27.0
- 1		1516 1518	580 B-#18	4051 4667	78.5 74.9	78.5	70.6	72.3	77.2	\$0.1	80.9	-1.6	15.0
•		1520 i	707	3932 4078	23.5	73:1	63.1 70.7	72.7	77:2	77.2	60. 4	-5.3	10.5
- 1		1523	720 747	4078 2570	10.2	87.8	78.5	82.5	23:3	3.3	33.6	-1.5 4	21.5 22.5
- 1		1533	DC-8	4300 L	88.0 79.4	95.1 79.3	74. 6 69.5		97.0 78.8	87.7	88. 4	- :	85.5 15.5
- 1		1534	DC-8	4256 3742	91.0 64.2	12: 7	74.3	73.8 82.1	86.2	80.0 92.0		6 -1.0	15.5
- 1		1537	727	3742 3867	84.2 82.0	82.0	71.0	76.6	82.7	13.4	99.7 94.6	-1.8	17.0 35.0
1		1542	720	4350	93.3	79.5	72.0 77.6	77.1 66.0	90.4	84.0	06.1	-2.0	13.0
ł		1547 1549	30-8 580	5364	12:3	8 1.3	69.9 70.3	76.0	82.5	35.0 86.6	92.4 95.3	-1.7 -1.7	15.0 17.4
1		1550	720	4514 4350	79.3 92.2	79.7 85.6	70.3 76.9	13.1	76.9	80.2	86.4	9	Hi
•					****	47.4	14.7	85.1	90.5	94.2	91.5	-2.0	11.7

TABLE V (Con't)

Pos	Date	Time	A/C	Distance Pt.	EPML RPMED	4EMEL	A-level dBA	D-level dNO	PALA PAGE	PHILIPM PHILIP	PHILC PHIEB	D 4B	d 800
D	67	1552 1641 1645 1812 1317 1838	727 727 BAC-111 DC-9 727 707	4377 3682 4195 5385 3053 4099	84.2 89.2 87.8 84.7 83.4 92.8	82.2 85.6 87.4 83.2 81.9 85.5	71.1 75.7 81.0 72.4 72.4 76.5	76.7 81.3 85.1 77.7 78.3	83.0 87.3 90.5 83.5 85.1 89.3	83.6 89,1 81.4 85.0 86.4 93.8	84.9 88.8 81.5 85.0 85.7 90.4	.6 .1 -3.6 3 -3.0 -1.0	22.5 22.5 14.0 22.5 17.0 17.5
D	6–7	1910 1922 1925 1927 2102	727 727 727 727 DC-8	4000 3515 4377 4112	84.1 80.1 78.9 80.7 82.0	81.7 79.2 77.5 79.7 78.6	70.6 67.2 66.6 68.4 69.2	76.3 72.3 72.5 73.7 74.1	82.8 77.9 78.1 79.2 81.0	84.7 78.6 79.0 79.9 83.1	84.1 79.5 79.4 80.1 83.7	6 1.5 1 .8 -1.1	25.0 35.5 24.5 27.5 20.5
ם	6-7	220 8 23 3 4			83.2 87.9	79.4 83.1	70.6 76.9	77.÷ 83.8	82.0 88.3	86.2 92.3	84.8 89.3	-3.0 -4.4	15.5 9.5
כ	€-9	1036 1043 1046 1047 1049			76.0 83.1 74.8 79.7 75.5	74.5 77.1 74.5 76.1 76.4	66.2 69.4 64.3 66.9 66.6	71.1 77.3 69.8 72.9 70.1	76.3 82.7 74.5 79.2 76.0	78.5 87.4 75.2 82.8 79.2	78.8 84.1 76.2 50.7 78.4	-2.5 -4.3 -3.1 -3.7	16.5 12.5 19.0 10.0 8.0
D	€-10	1945 1959 2046 2058 2136	580 727	4270 3362	70.1 82.8 77.5 88.7 73.7	73.5 82.9 78.3 87.4 73.0	64.4 72.4 66.0 76.5 62.0	66.6 76.4 69.0 81.3 66.8	70.4 81.5 74.2 87.3 71.3	73.7 52.3 76.3 89.6 72.6	75.2 82.9 76.0 88.2 74.3	-3.6 .5 1.2 9 1.1	11.0 25.5 35.0 23.0 23.0
ū	6-10	2204 1420 1500 1557 1608 1708 1732 1852	727 VC-10 707 747 727 707	5043 5255 5596 3433 42.8 4619	70.2 75.1 83.0 66.3 84.8 80.3 91.8 72.8	71.0 77.8 82.9 69.5 83.6 79.1 85.4 72.8	63.5 67.0 73.8 63.2 73.2 67.5 77.3 63.5	68.6 71.4 77.6 67.7 77.8 72.9 85.5 69.9	72.2 76.4 82.9 71.9 83.2 78.8 89.7	72.9 77.2 83.1 71.9 85.1 79.4 94.5 79.6	73.6 77.8 84.2 76.2 84.6 79.6 91.1 78.8	-2.7 -2.1 1 -5.6 3 .9 -2.7 -6.8	17.0 15.5 23.0 6.0 19.5 30.0 13.5
С	6-11	1910 1914 1921 1941 1948 1951 2010 2013 2032 2107 2146 2151	707 727 727 727 727 727 727	5196 4218 3013 3625 3803 6629	90.3 87.6 84.7 80.9 84.3 79.5 84.3 77.1	83.7 77.8 84.4 92.2 79.3 81.1 79.5 64.9 81.4 75.9	75.9 65.2 74.5 71.5 69.4 69.7 67.8 70.8 71.4	84.0 70.4 81.0 78.0 75.1 75.6 72.8 74.8 65.3 77.2	89.70.551.6551.6551.6551.6551.6551.6551.6551	93.7 77.4 89.3 87.5 77.8 81.2 79.1 80.8 70.3 84.9	90.969.1958.86.3858.870.8858.70	-3.4 1.8 -1.7 -2.8 2.8 3 .7 2.2 -1.1 -7.8	12.0 34.0 19.0 18.5 36.0 29.5 17.0 22.0 23.5

TABLE V (Con't)

And the second s

Pos	Date	Time	A/C	Distance Pt.	EPHL EPHES	SENEL 48	A-level	D-lovel	PHILM PHAR	PHI/PH PHAS	PHLC PHAB	D 43	4
E	6-2	1552 1618 1647 1652 1715 1717 1835	72" 7".1 DC-9 727 720 727	4350 3252 4621 3480 4398 4000	80.1 91.0 78.7 88.0 83.6 75.3 82.9	78.7 88.5 76.7 84.1 83.2 75.7 78.8	68.2 77.8 66.7 75.0 74.8 69.2 69.3	73.0 82.9 71.8 80.8 82.7 74.0 74.8	78.4 89.1 78.6 87.6 86.7 79.5	79.5 09.7 73.2 08.2 91.5 09.2 83.0	81.3 91.5 79.8 88.2 88.8 82.6 81.9	.6 .3 5 2 -7.9 -4.9	20.5 34.0 24.0 25.5 4.0 9.5 18.0
E	6-3	1415 1417 1419 1427 1516 1522 1524 1527 1539 1714 1741 1821	DC-8 727 DC-9 707 VC-10 747 DC-8 727 707 727 727	5659 5523 3976 4004 4051 4058 3987 3987 3782 3968 4350 3702	78.6 77.7 79.5 92.2 80.3 84.7 86.6 88.7 80.8	74.6 76.3 81.1 77.5 85.7 83.3 84.5 81.3 73.1 83.5 82.0	66.4 66.0 71.5 69.3 77.9 73.7 74.4 71.6 63.4 73.7 66.9	73.0 71.1 78.0 74.2 86.1 78.6 79.6 81.8 76.2 67.5 80.4 76.4	79.1 77.2 85.0 80.2 91.2 85.6 88.0 72.1 78.1	82.4 167.6 81.6 95.27 89.6 89.2 89.2 99.1	80.0 78.5 81.5 92.8 87.8 86.2 73.2 89.8	-3.8 -2.9 -1.5 -3.3 -5.2 -1.4 -4.3 -2.2 1.0	12.0 21.0 14.5 18.0 12.5 8.0 18.5 12.0 20.5 19.0 24.5 26.0
E	6-3	1934 1944 2136 2146	.'20 727	4036 5194	82.9 76.4 81.2 78.9	80.3 77.2 77.5 75.0	72.8 67.5 64.4 64.8	80.1 72.6. 70.6 72.0	83.5 77.3 77.0 76.2	86.0 77.8 81.2 79.8	85.3 79.1 78.7 77.8	-3.1 -1.4 0 9	13.5 18.5 21.0 22.0
E	6-3 6-4	2259 0802 0850 0918 0929 1526 1528 1533 1543 1547 1547	720 DC-9 727 BAC-111 727 747 720 727 727	4036 5108 4686 5058 4405 7113 3764 3824 4350 4142	67.9 83.9 76.9 74.8 76.2 77.1 81.2 88.7 80.9 71.6 77.6	69.3 79.4 77.2 75.5 75.4 75.9 77.8 82.8 80.2 71.4 77.2	59.5 70.6 67.0 63.7 63.7 67.3 68.7 68.7 68.7 68.7	64.2 77.8 71.7 68.7 69.1 73.8 82.3 73.8 73.8 74.3	68.3 81.9 76.8 73.1 74.8 75.3 87.4 77.8 77.8	68.8 85.5 77.8 77.8 77.6 82.5 91.5 77.8 77.8 77.8	69.9 84.1 79.6 74.3 77.5 81.9 81.9 79.5 81.9	9 -1.6 6 1.0 .7 -1.3 -2.4 -6.2 6	18.0 18.5 20.0 33.5 34.0 26.0 19.5 12.5 22.0 7.5 22.0 22.5

TABLE V (Con't)

Pos	Date	Time	A/C	Distance Ft.	EPHL EPHAB	SEMEL, 48	A-level dBA	D-level	PHEAT	PHEATH	PHLC	D 48	4
•	6-5	1059 1102 1105 1107 1112 1116 1119 1405 1421 1425 1717 1719	737 DC-8 DC-9 707 727 737 DC-8 BAC-111 DC-8 707	3992 3474 3615 5017 4243 3770 3967 3850 3847 2596	78.3 93.6 81.2 90.4 80.9 77.2 79.1 73.9 81.8 90.1 90.7	77.2 86.4 78.4 85.2 80.0 75.5 78.1 74.2 79.6 84.4 87.6 85.1	66.1 77.4 78.2 73.5 69.1 66.4 64.1 68.2 75.0 80.6	69.6 85.5 75.0 81.0 74.3 70.7 68.7 73.7 82.4 85.7	75.7 91.7 80.5 87.2 80.1 75.7 76.2 74.5 79.9 88.9 89.6	78.6 94.5 82.2 81.1 77.3 78.6 74.5 92.6 94.1	76.5 92.4 89.5 81.6 78.2 79.0 82.1 90.9 91.0	3 -1.0 2 1.5 5 5 -2.4 -3.4	23.0 18.5 18.0 24.5 22.0 26.5 28.0 22.0 28.0 13.5 11.0
7	6-5	1953 2114 2126 2139			91.6 81.2 86.9 85.3	87.6 79.4 82.2 81.7	78.0 68.6 73.0 71.5	84.2 73.7 79.7 78.2	91.2 79.0 86.0 83.7	92.4 81.8 89.8 86.4	92.2 80.3 87.9 85.9	8 6 -2.9 -1.1	16.0 21.5 19.5 19.0
,	6-5	2256			98.2	82.2	72.6	80.6	85.2	90.3	87.3	-2.1	19.5
P	6-6	0701 0849 0941 0938 1024 1038 1050 1054 1056 1138 1817 1615 2007 2008	DC-8 727 720 720 727 727 727 720 727 720 727 720 727 720	5382 4046 3813 3591 4500 3610 3659 3375 4192 5591 3516 420%	846.3537 8 817.88.88 817.88 817.88 817.98 817.98 817.98 817.98 817.98 817.98 817.98 817.98 817.98 817.98 817.98 817.98 817.99 818.88 81	78.9 76.7 79.4 82.1 78.4 61.1 81.7 75.3 81.7 76.8 78.6 81.1	76.2 65.7 65.7 74.5 70.7 77.8 73.2 71.3 75.7 67.6 70.0	77.9 70.2 74.2 81.7 75.1 86.6 80.6 77.2 80.2 79.9 72.8	83.54 75.436 80.694 80.28 81.52 78.8 81.8	87.6 75.7 81.7 81.9 81.2 988.3 84.7 90.0 86.5 81.3	84.5 782.13 87.43 81.3 81.3 86.5 86.5 86.7 81.5 81.5 81.5 81.5 81.5	-3.1 2 -2.6 -3.2 -2.0 -2.2 -2.0 -3.1 -2.1 -1.7	12.5 25.0 24.0 12.5 15.5 16.5 17.0 17.0 17.0 32.5 15.0 20.5 20.5
F	6-7	075578 075578 08048 0814258 08228 08228 08334 08334 08334 0844 10012 1004 1005 1100 1100 1100 1100	720 727 727 720 727 707 720 Lear 707 727 737 727 727 727 727 727 727 580 DC-9 727 580 DC-9 737 737	37177074 38084 50808	80.900 85.22 85.22 88.72 88.72 88.72 80.28 774.18 774.18 774.18 80.00 86.03 774.18	79.666639877756.666339877756.613856427798777628.8987758.88.89877628.8987788.8987788788.8987788788.8987788788.8987788788.89877788768.8987788788.8987788788.8987788788.8987788788.8987788788.8987788788.8987788788.8987788788.8987788788.8987788788.8987788788.8987788788.8987788788.8987788788.8987788788.8987788788.89887888.8988788888888	69.39.37.4.2.6.5.37.4.5.0.0.0.4.9.0.5.4.5.5.3.3.8.2.3.3.7.4.5.0.0.0.4.9.0.5.2.4.5.5.3.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5	74.5 78.7 78.7 78.7 78.7 78.7 78.7 67.5 69.8 77.6 77.6 69.1 77.6 69.1 77.6 71.2 71.4 80.7 71.8 77.8 77.8 77.8 77.8 77.8 77.8 77	82.9753996988227583996983523.998482283983523399633667745.89849636677955877557765779877987798779877987798779877987798779	81.57.538.985.792.385.985.985.985.985.985.985.985.985.985.3866.74.0886.78.3866.7866.7	82.23 84.33 86.33 86.39 86.39 87.73 81.8 87.8 81.8 83.6 83.6 83.6 83.6 83.6 83.6 83.6 83	1.7 66 - 4.3 7 - 2.5 66 3 - 2.16 8 - 1.7 - 1.8 - 1.9 - 1.8 - 1.8 - 1.8 - 1.7 - 1.8 - 1.8 - 1.8 - 1.7 - 1.8 - 1.	26.5 31.5 31.5 21.5 21.5 21.5 21.5 21.5 23.0 28.5 29.5 27.5 27.0 23.5 27.0 23.5 27.0 23.5 27.0 23.5 27.0 27.5 27.5 27.5 27.5 27.5 27.5 27.5 27.5

Pos	Date	Time	A/C	Distance Pt.	EPIR.	STATE L	A-level	9-level	PHEA PHAD	PHILIDO Phopo	PHIC	D dB	4
•	6-7	1105	DC-8	3012	91.9	84.7	75.0	63.3	89.2	93.1	90.2		
	ĺ	1107 1109	727 720	37 02 3693	70,5	77.9	66.1	72.0 66.1	77.7	78.2	79.0	-1.2 .3	26 .0 23.0
	Į.	1116	,	3093	92.1 78.0	85.6 77.5	77.7 67.3		90.4	95.0	91.4	-2.9	13.0
	l	1116	720	6314	78.4	74.5	65.9	70.3 72.4	75.9 78.1	79.1 81.7	78.5 79.2	-1.1 -2.9	17.0
		112 6 112 8	580 DC-9	4309 3717	75.1 85.4	76.2	65.8 C6.8	69.6	75.4	78.5	77.4	-3.4	11.0 14.0
		1143	727	4800	12.4	8 1.2 8 0.0	71.1 68.7	78.1	84.3 79.5	95.4	85.4	0	23.5
	ŧ	1146 1147	Lear B-80	4607	64.8	6 9 .7	60.6	73.9 64.5	69.I	6 0.7	82.1 72.4	1.7 -5.1	31.0 10.5
		1150	DC-9	5175 4170	74.6 80.1	72.7 78.4	62.9	71.6	75.3	76.5	78.8	-1.9	16.5
		1158	DC-9	3800	77.4	75.8	68.9 65.8	75.2 70.9	81.0 76.9	82.6 78.4	3.2	-2.5	12.0
		1215 1230	Jet Star DC-9	1905	82.3 81.4	8 2.6	73.0 68.7	76.8	\$1.5 80.6	82.0	80.5 84.5	-1.0	25.0 23.5
		1251	727	4275 4080	78.2	78.9 78.5	68.7 68.5	75.1		82.2	82.7	- :8	20.5
		1251 1309	580	7537	71.0	78.4	69.2	73.4 72.7	78.3 77.7	78.8 61.2	80.3	6 -10.2	18.5
		1321 1326	DC-9 737	3076 4052	82.4	78.6	72.5	78.9	85.5	67.1	79.9 85.7	-4.7	2.0 10.0
		1338 1342	DC-9	3600	73.4 83.4	75.2 80.5	64.7 71.4	69.9	75.7	76.6	77.3	-3.2	15.5
- 1		1342	727	334£	82.5	81.3	71.5	77.8 76.6	84.0 81.5	85.2 81.9	#5.0 #5.0	-1. 8	15.0
- 1		1359 1405	DC-9 727	4215 391↑	78.1	76.0	66.0	71.6	78.0	78.9	80.1	- :8	24.0 21.5
		1411	DC-8	8430	81.4 88.4	79.9 83.0	69.9 72.3	74.9 79.3	80.1	61.2	81.7	.2	21.5
		1413	707	3032	86.6	82.3	74.0	81.7	86.0 86.4	89.0 90.1	87.1 87.6	6 -3.5	20.0
		1417 1420	727 DC-8	3824 3611	82.0	79.7	71.0	76.4	82.2	83.1	82.9	-1.1	12.5 20.0
1		1422	B-80	5175	88.3 61.1	82.7 76.1	74.3 67.7	81.3 75.4	87.1	89.2	87.8	9.	24.0
1		1426	727	4533	90.2	86.4	75.1	80.7	81.8 87.6	61.6 89.4	83.8 90.0	7 .8	17.5 27.0
- 1		1434 1445	DC-8 727	3660 3777	91.6	85.0	76.4	84.0	90.6	93.1	91.4	-1.5	21.0
ļ		1501	VC-10	437A	73.5 84.2	77.6 83.6	67.7 76.9	72.2 81.7	78.9	80.1	80.7	-6 .6	4.0
1		1517	580	1855	82.7	81.5	71.7	75.4	87.3 81.5	88.1 63.1	89.2 83.9	-3.9	9.5 17.0
- 1		1520 1523	707 720	3622 3600	93.9 87.8	87.3	76.9	85.2	90.5	94.4	92.1	4	23.0
- 1		1535	DC-8	7897	85.7	86.9 81.3	75.5 70.5	79.9 78.0	85.2 83.7	86.0 88.3	87.1	1.8	33.0
- 1		1537 1540	727	3722	83.0	80.9	70.3	75.4	81.9	82.7	86.6 83.3	-2.6	15.0 24.0
- 1		1542	727 720	3728	84.7 94.3	82 * 87.1	72.4	77.4	84.1	85.3	83.3 85.8	.3 6	25.5
- 1		1547	DC-8	371€	85.9	81.1	79.2 68.8	87.5 74.8	92.4 81.9	97.0 85.8	93.5 84.9	-2.7	13.0
- 1		1548 1551	580 720	3822 3501	81.9	79.3	70.0	72.5	78.3	\$1.7	80.9	.1 .2	26.0 22.5
- 1		1557	727	3824	91.2 82.1	84.6 80.2	76.0 69.6	84.0	89.2	92.7	90.4	-1.5	16.5
		1556	727	ANHE	81.4	80.0	69.3	75.1 74.8	81.3 81.2	82.1 81.3	\$1.9 83.6	.1	27.5
- 1		1610 1626	737 BAC-111	3575	74.4	73.8	64.7	69.3	74.9	75.6	77.2	-1.2	17.0 19.5
ı		1640	727	3252	76.5 86.4	77.4 83.1	66. 8 72.1	74.6 78.0	78.5 84.4	81.0	84.3	-4.5	11.0
- 1		1647	BAC-111	3704	88.1	86.5	77.4	81.9	87.5	86.3 88.8	89.5	7	28.5 27.5
- 1		1654 1758	727	4971	75.9 79.7	72.7	67.3	75.6	79.8	81.4	80.9	-5.5	6.5
- 1		1812	DC-9	3931	84.3	78.6 82.2	70.9 71.9	76.6 77.5	82.2	03.6	3.2	-3.9	13.0
- 1		1843 1844	1	1	76.8	78.6	69.9	74.4	83.9 79.4	86.7 79.4	8 5.7 8 1.3	-2.4 -2.6	10.5 11.5
.]			J.	_ j	82.2	00. 0	70.1	75.9	81.8	83.0	83.4	8	20.0
' [6-7	1901	720 DC-4	4833	82.5	77.9	68.5	75.5	80.2	82.4	82.4	.1	23.0
- 1		1931	727	4275 3061	76.0 83.7	75.4 81.4	64.3 70.2	69.2	74.7	74.7	76.4	1.3	29.0
- 1		1947	727	1700	78.3	78.0	67.3	76. 8 71.7	83.7 77.1	84.2 77.7	84.9 79.0	5 .6	23.0
- 1		1957 2000	I	ì	79.9	80.4	7.8	75.0	80.0	80.5	81.6	6	24.0 26.5
1		2008	1	Ī	81.4 79.3	79.7 78 .4	69.7 69.0	75.5 74.1	81.9	83.5	83.8	-2.1	17.5
- 1		2012	1	i	70.9	75.6	65.2	74.1 72.4	78.9 77.5	80.0 7 8. 9	80.8 80.9	7 -8.0	17.0

TABLE V (Con't)

Pos	p3te	Time	A/C	Distance Pt.	ephi. Ephad	SEMEL 48	A-level	B-level	PHLM PH4B	PHLIN PHGB	PHEC PHAR	D 49	d 300
P	6-7	2023 2101 2103 2149			86.4 84.1 92.1 78.6	81.9 80.0 85.2 74.8	69.8 72.4 77.5 63.0	76.4 76.5 85.9 70.4	83.7 84.0 90.0 75.4	85.5 87.5 94.7 79.5	85.0 85.6 91.0 78.4	-3.4 -2.6 9	38.5 12.0 11.0 23.5
7	6-7	2200		İ	83.5	79.7	_e 69.7	75-9	82.0	85.6	83.2	-2.1	19.5
7	6-8	1035 1043 1051			78.1 85.3 79.4	76.4 79.5 78.3	67.6 72.6 70.0	73.8 80.3 74.7	79.5 85.1 80.6	80.9 89.0 82.5	79.9 86.1 81.6	-2.8 -3.7 -3.1	16.0 12.0 13.5
7	6-10	1959 2046 2058			81.6 70.1 87.5	81.7 78.3 86.3	70.9 67.7 75.6	75.0 72.4 79.6	80.5 77.1 85.7	81.5 77.9 88.8	82.9 80.9 87.4	-6.8 -1.3	22.0 4.5 22.0
P	6-10	2207	1]	78.5	79.2	69.1	73.5	78.2	78.9	79.1	4	27.0
P	6-13	1852 1854	720 EAC-111	4.60	78.0 73.9	7f.5 75.2	67.6 64.7	78.7 69.3	82.1 74.8	83.7 76.0	85.3 77.9	-5.7 2.1	7.5 14.5
Đ.	6-11	1908 1908 1911 1911 1941 1944 1947 1947	DC -8 725 727 727 727 727	4197 F/24 4197 9894 9813	86.8 73.2 92.1 76.0 86.3 86.1 51.5 91.3 84.8	82.2 73.2 85.5 73.2 83.4 74.6 78.9 81.5	71.6 65.7 78.9 71.7 67.7 72.8 72.0 67.5 67.5 70.8 68.5	79.5 71.4 86.5 77.1 77.0 75.3 80.5 78.1 72.2 73.6 77.1	84.7 78.0 90.0 80.2 82.6 79.2 81.9 77.6 80.0 83.5 80.3	89.1 79.6 95.9 83.6 80.2 78.6 80.1 80.1 80.1 80.8	88.6 80.12 85.4 85.5 85.5 85.5 85.5 85.8	-2.3 -6.4 -3.8 -7.7 0 -4.5 -3.1 -2.6 1.2 -1.4 2.0	16.5 6.0 10.0 3.5 21.0 6.0 15.5 13.5 24.0 27.0 20.0 32.5

taken at the individual sites. In identification, no attempt was made to distinguish between the various models of 707 and DC-8 type aircraft or to distinguish between turbojet and turbofan models.

Distance information was established from the photographs after identification of the aircraft and from knowledge of key dimensions of the aircraft. Photographs were taken at the ground position essentially at the point of closest approach of the aircraft to the observer.* Although distance information is reported in four significant figures in Table V, accuracy is limited to the order of ±5%.

For the measurements, the distance from the ground observer to point of closest approach is equivalent to the slant distance which may be defined as the length of an imaginary straight line passing through the point of interest on the ground and the aircraft flight path, which forms the hypotenuse of the vertical right triangle whose legs are normal to the flight track on its tangent. The slant distance and distance to point of closest approach are nearly equal because of the relatively small descent angles involved.

The noise measures tabulated in Table V are identified as follows:

Measure	Unit	Meaning
EPNL	EPNdB	Effective perceived noise level calculated in accordance with FAR Part 36.4/ The EPNL is equal to: EPNL = PNLTM + D.
SENEL	₫B	Single event noise exposure level as defined in Reference 5 with the exception that the summation included only the upper 10 dB of the flyover noise signal.*
A-level	dBA	A-weighted sound level as specified in USA standards for sound level meters, S1.4.7
D-level	dBD	D-weighted sound level as specified in SAE ARP 1080.2 For many flyover signals, the following approximate relationship holds. PNIM = D-level + 7
PNLM	PNdB	Maximum perceived noise level as defined in FAR Part 36.
PNLTM	PNdB	Maximum tone-corrected perceived noise level as defined in FAR Part 36.
PNLC	PNdP	Composite perceived noise level, computed from the highest levels reached in each of the one-third octave frequency bands irrespective of time. 9/
D	đB	Duration correction as defined in FAR Part 36.
đ	sec	Duration time as defined in FAR Part 36.

^{*} SENGL is defined in terms of integration (summation) from a threshold noise level approximately 30 dB below the maximum level. However, integration over only the upper 10 dB results in values that typically differ by 0.3 dB or less from values based on integration over 30 dB.

IV. EPNL AND NEF COMPUTATIONS AND COMPARISONS

Mean EPNL and NEF values calculated from the measured noise data are given in the later part of this section. The mathematical basis for calculating these noise values is summarized in the first part of this section.

A. NEF and EPNL Equations

The noise exposure forecast procedures yield estimates of the noise exposure based upon consideration of the noise levels, expressed in EPNdB, the number of noise intrusions and the time of day in which the noise intrusions occur. The contribution to the NEF value at a given position for a given day for a single flyover event, i, may be expressed as follows:

$$NEF(i) = EPNL(i) + 10 log K(i) -88$$
 (Eq. 1) where

EPNL(i) = effective perceived noise level produced by flyover (i).

K(i) = 1, for times between 0700 to 2200

K(i) = 16.67 for times between 2200 to 0700.

When a number of noise intrusions of differing levels occur during the day, the noise exposure forecast value for a given position and day may be expressed as:

NEF = 10 log
$$\sum_{i=1}^{N}$$
 antilog $\frac{NEF(1)}{10}$ (Eq. 2)

or, NEF = 10 log
$$\sum_{i=1}^{N}$$
 antilog $\left(\frac{\text{EPNL}(i) + 10 log K(i)}{10}\right)$ -88 (Eq. 2a)

where $N = N_D + N_N$

 N_D = number of events between 0700 to 2200

 N_N = number of events between 2200 tc 0700

For the rather special case where the same noise level is produced by a number of events, Equation 2 becomes:

$$NEF = EPNL + 10 log [N_D + 16.67 N_N] -88$$
 (Eq. 2b)

As can be seen from Equation 2b, in particular, the NEF values are significantly affected by the number and time of the noise occurrences as well as the noise level.

In determining the changes in noise environment due to the changes in approach procedures at DTW, the changes in noise levels and the corresponding change in NEF values are of primary interest. The large variability in the number of IFK approaches on Runway 21R may be considered to be an uncontrolled "random" test variable, which, through its influence on NEF values, might well obscure NEF changes due to changes in noise levels. Thus, to provide meaningful comparisons of noise exposure between test phases, one wishes to determine "mean" noise levels, for the various test days and test phases. various mean noise levels can also be used in adjusting "raw" NEF values to account for flights occurring between 2400 and 0600 that were not measured. From mean noise level values, one can also establish the differences in NEF values which result from differences in noise levels, un-obscured by the wide variation in number of events occurring during particular test periods.

In determining mean noise level values for NEF computations, the "energy mean" value will be of primary interest, reflecting the fact that the sound pressure noise levels are expressed as logarithms of the sound pressures involved. The energy mean value, EPNL, (termed "mean" throughout the remainder of the report) can be defined as:

$$\overline{EPNL} = 10 \log \frac{1}{N} \sum_{i=1}^{N} \text{ antilog } \frac{EPNL(i)}{10}$$
(Eq. 3)

If the mean EPNL is first calculated from all the noise events measured during a certain period during the day, the NEF value may then be estimated from Equation 2b, using EPNL from Equation 3:

NEF =
$$\overline{EPNL}$$
 + 10 log [N_D + 16.67 N_N] -88 (Eq. 2c)

The above expression will serve as the major equation for calculating NEF values from the experimental data.

The standard deviation is a commonly used statistical measure of the variability of a distribution of numbers. The standard deviation for $\overline{\text{FPNL}}$, $\overline{\text{s}}$, may be defined as:

$$\bar{s} = 10 \log \left\{ 1 + \frac{\left[\frac{N}{\sum_{i=1}^{N} \left(\frac{EPNL(i)}{10} \right)^{2} - \left(\frac{N}{\sum_{i=1}^{N} antilog} \frac{EPNL(i)}{10} \right)^{2} - \left(\frac{N}{\sum_{i=1}^{N} antilog} \frac{EPNL(i)}{10} \right)^{2} \right]}{\frac{1}{N}} \right\}$$

$$= 10 \log \left\{ 1 + \frac{\left[\frac{N}{\sum_{i=1}^{N} antilog} \frac{EPNL(i)}{10} \right]^{2} - \left(\frac{N}{\sum_{i=1}^{N} antilog} \frac{EPNL(i)}{10} \right)^{2} - \left(\frac{N}{\sum_{i=1}^{N} antilog} \frac{EPNL(i)}{10} \right)^{2} \right]}{\frac{1}{N}} \right\}$$

$$= 10 \log \left\{ 1 + \frac{\left[\frac{N}{\sum_{i=1}^{N} antilog} \frac{EPNL(i)}{10} \right]^{2} - \left(\frac{N}{\sum_{i=1}^{N} antilog} \frac{EPNL(i)}{10} \right)^{2} - \left(\frac{N}{\sum_{i=1}^{N} antilog} \frac{EPNL(i)}{10} \right)^{2} \right]}{\frac{1}{N}} \right\}$$

$$= 10 \log \left\{ 1 + \frac{\left[\frac{N}{\sum_{i=1}^{N} antilog} \frac{EPNL(i)}{10} \right]^{2} - \left(\frac{N}{\sum_{i=1}^{N} antilog} \frac{EPNL(i)}{10} \right)^{2} - \left(\frac{N}{\sum_{i=1}^{N} antilog} \frac{EPNL(i)}{10} \right)^{2} \right]} \right\}$$

$$= 10 \log \left\{ 1 + \frac{\left[\frac{N}{\sum_{i=1}^{N} antilog} \frac{EPNL(i)}{10} \right]^{2} - \left(\frac{N}{\sum_{i=1}^{N} antilog} \frac{EPNL(i)}{10} \right)^{2} - \left(\frac{N}{\sum_{i=1}^{N} antilog} \frac{EPNL(i)}{10} \right)^{2} \right\}$$

Although not of immediate interest, but likely to be of concern in other analyses of the noise and distance information, the arithmetic mean of the EPNL values may be defined as:

$$EPNL_{ave} = \frac{1}{N} \sum_{i} EPNL (i)$$
 (Eq. 5)

The mean level (Eq. 3) will always be equal to, or greater than, the arithmetic mean (Eq. 5):

The standard deviation for the arithmetic mean, s, is defined as:

$$s = \begin{bmatrix} \frac{1}{N} & \sum_{i} & \left(\text{EPNL(i)} \right)^{2} - \left(\sum_{i} & \text{EPNL(i)} \right)^{2} \\ \frac{1}{N} & \sum_{i} & \left(\text{EPNL(i)} \right)^{2} - \left(\sum_{i} & \text{EPNL(i)} \right)^{2} \end{bmatrix}$$
(Ea. 6)

To illustrate the differences between values computed on an energy or arithmetic basis, the following table shows the mean values and standard deviations computed for four noise levels of 90, 94, 96 and 100 EPNdB.

Quantity	Value	<u>Fquation</u>
EPNL s	96.4	3 4
EPNLave	95.0	5
s	4.2	6

B. Mean Noise Levels

Table VI lists the mean noise revels, calculated in accordance with Equation 3, for each day at each position. Mean levels are also listed for each phase of measurement at each position. Also shown are the mean levels at each position during the two phases for: four-engine jet aircraft, two- and three-engine jet aircraft and propeller aircraft. The table also lists standard deviations, calculated in accordance with Equation 4.

The mean noise levels for each day are also shown in Fig. 6 together with the standard deviation for each day. The dashed lines in the figure show the mean values for the entire test phase at each position.

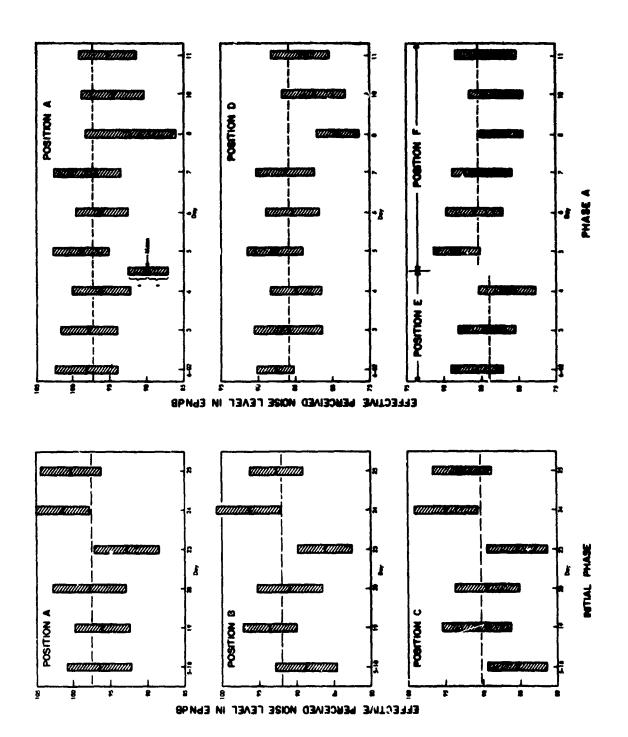
At position A, note the very small difference (0.3 dB) between mean EPNL values for the two measurement phases. Also note that the differences in mean values t position A were also quite small for the four-engine jet aircraft (1.0 dB) and for the two- and three-engine jet aircraft (1.3 dB).

C. Daily NEF Values

NEF values, calculated from the mean noise levels in accordance with Equation 2c, are tabulated in Table VII and are also shown graphically in Fig. 7. Table VII lists two sets of NEF values. The "raw" values are based upon the mean noise levels and the observed number of flights during the observation periods from 0600 to 2400. "Adjusted" NEF values are also shown; these values reflect adjustments for the IFR landings on runway 21R occurring between 2400 and 0600 which were not measured.

TABLE VI MEAN EPPECTIVE PERCEIVED NOISE LEVELS

Test Phase	Aircraft	Period	L EPN4B	SPNdB	ជ	EPN4B	EPNdB	æ	T EPNdB	S EPN43	c	edata I	EPMAR	E
				4			В			O				
Initial	A11	May 18		•	137	88.7		58		0.4	300			
		20			2 2 2	93.5		187	•	90 a	* £			···
		23		•	35	86.1		6.a		, rd , at	139			
		25 76 18-25	100.3	มฐ กูญษ์	25 to 15 to 25 to	92.6 92.6 91.6	ร พร พูงอ	29 164	92.3	a wro violi	26 176			
	4-Eng. Jet	F F	100.6	4.6		94.7	4.2		0.400	8.2				
	Prop	E	77.78			`	•		ا∞ر	• •				
				¥			a			ſĸ			8.	
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The second of th

TABLE VII
DAILY NOISE EXPOSURE FORECAST VALUES

Test Phase	Period	NEF Values							
		RAW	ADJ	RAW	ADJ	RAW	ADJ	RAW	ADJ
		Þ		В		С			
Initial	5-18	32.5	36.7	21.4	25.7	18.0	22.7		
	5-19	32.7	36.2	25.9	31.2	22.6	28.3		
	5-20	32.5	36.7	23.2	27.1	22.6	26.5		
	5-23	28.1	28.1	18.2	18.2	16.3	16.3		
	5-24	33.5	33.5	26.3	26.3	25.5	25.5		
	525	37.4	40.9	25.7	29.8	28.8	32.2		
	Ave*		36.8		27.8		27.5		
			Ą	.:		E		F	
A	6-3	36.1	37.8	19.5	21.6	18.6	20.5		
	6-4	30.6	36.4	15.3	21.4	12.1	18.0		
	6-5	34.5	34.5	18.0	18.0			18.2	18.2
į	6-6	33.0	33.0	19.0	19.0			16.6	16.6
}	6-7	35.6	37.2	20.2	22.2			19.1	21.4
	6-8	19.5	19.5	1.9	1.9	}		6.7	6.7
	6-10	25.5	25.5	10.7	10.7			11.2	11.2
	6-11	27.7	27.7	12.7	12.7			14.4	14.4
	Ave##		34 - 9		19.5		19.4		17.6

^{* &}quot;Energy" average for six days.

[&]quot;Energy" average for seven days for positions A and D, excluding data for 6-8 and 6-9; averages for two days only at Position E, and for five days at Position F, excluding data for 6-8 and 6-9.

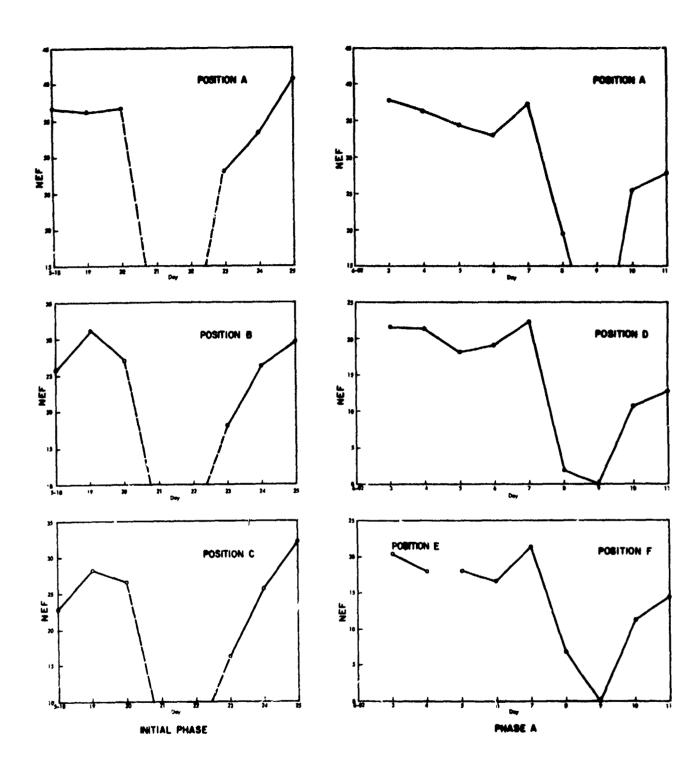


FIGURE 7. DAILY NOISE EXPOSURE FORECAST VALUES

The number of IFR flights between 2400 and 0600 and type of aircraft were determined by review of FAA traffic control "flight strips". The adjustments take into account both the number and the type of aircraft.* It will be noted that even though the number of approaches during 2400 and 0600 was small, the adjustments were sometimes significant because of the high weighting assigned to night flights in the NEF calculation procedures.

D. Mean NEF Values

Table VII also lists mean NEF values for the two test phases. These means are calculated in accordance with Equation 2, but include NEF values only for the days in which there are appreciable number of IFR approaches on runway 21R. Thus, for the initial phase, the mean value is based upon six days of measurements, omitting the almost neglible NEF values for May 21 and 22. On a similar basis, the mean NEF value for Phase A is based on several daily NEF values, omitting data for June 8 and 9 when very few noise events were noted.

^{*} Noise levels were estimated for individual flights between 2400 and 0600 by assuming, first, the mean level observed for all flights during that day, and then adding to this value, the difference between the mean value for the test phase and the test phase value for the type of aircraft involved. Thus levels were adjusted to account for differences in noise produced by four-engine, two- and three-engine jets and propeller aircraft.

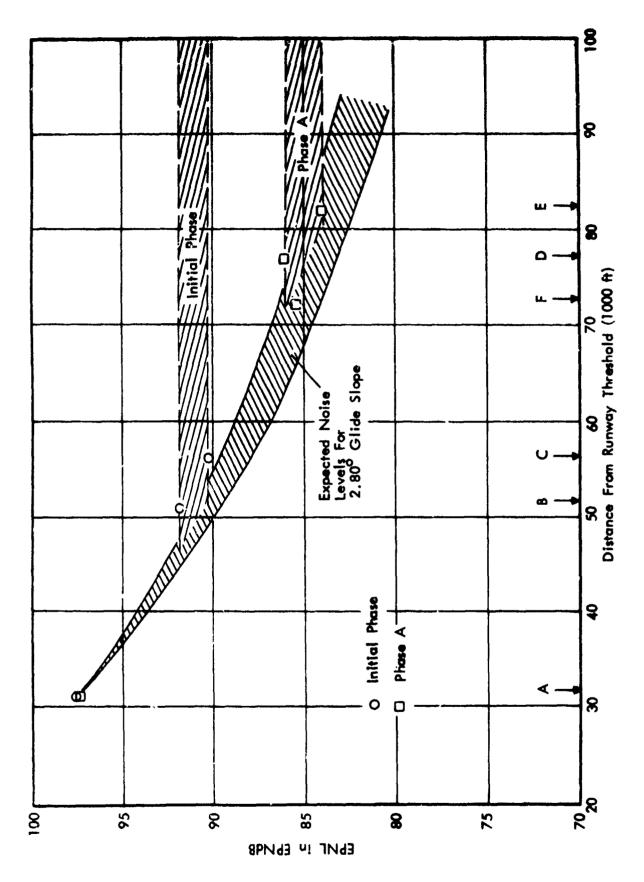
V. COMPARISON OF NOISE LEVELS AND NOISE EXPOSURE BETWEEN TEST PHASES

The most direct comparison of differences in noise exposure due to test conditions is in terms of the mean noise levels observed at the different position. This comparison largely avoids variability introduced by the daily variations in the number of flight operations. However, a meaningful comparison of adjusted NEF values may also be obtained when the values are adjusted to a common volume of operations.

Figure 8 compares the mean noise levels for the two test phases. In this figure the mean noise levels from Table VI for each test phase are plotted as a function of the distance from the runway threshold. (Measurement positions may be identified in the figure.) The figure shows the very close agreement in mean noise levels (within 0.3 dP) observed at position A.

To illustrate the typical variation in noise levels for aircraft following the 2.8 degree glide slope at a constant thrust setting, two curves have been drawn through the noise levels at position A. In the figure, the difference between the curves is shaded. The upper curve assumed that the EPNI, values decrease at a rate of 9 EPNdB per doubling of distance; the lower curve assumes a decrease of 11 EPNdB per doubling of distance.

Intersecting the two curves are horizontal lines bracketing the effective perceived noise levels measured at positions B and C in the initial phase and positions D, E and F in phase A. The difference between the two horizontal shaded areas represents, approximately, the reduction in noise levels between the test phases.



COMPARISON OF MEAN EFFECTIVE PERCEIVED NOISE LEVELS FOR THE INITIAL PHASE AND PHASE A TESTS . ω FIGURE

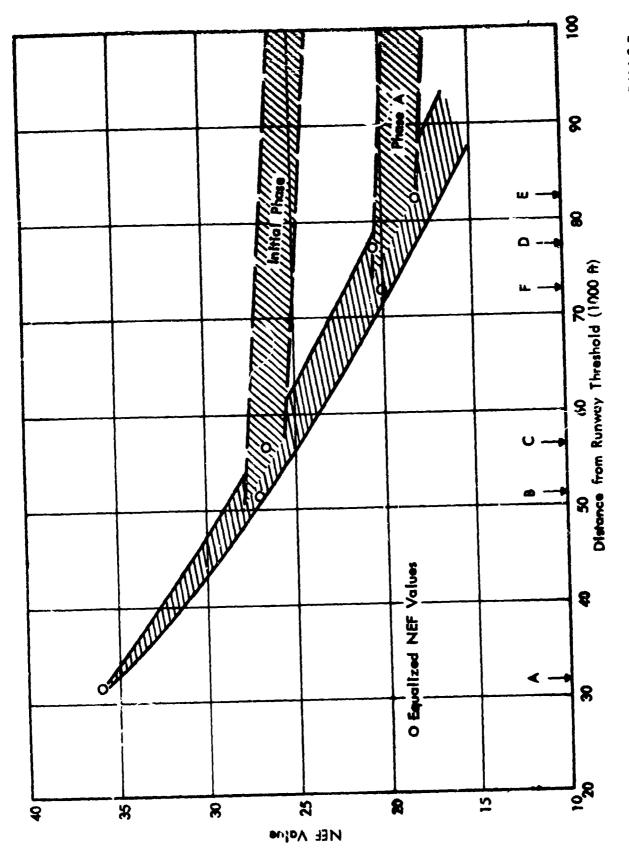
At distances from the runway threshold 90,000 ft and greater this net difference is approximately 6 EPNdB. This value is slightly greater than that expected from a typical EPNL versus distance curve, considering a simple change in slant distances from 2400 to 3400 ft AGL. Hence the test noise level comparison shows net noise reductions that slightly exceed simple estimates based on previous noise level information.

To reduce variations in NEP values due to test differences in volume of operations, a set of "equalized" NEP values has been computed from the NEF values of Table VII. These values are listed in Table VIII, and are also plotted in Fig. 9 as a function of measurement distance from the runway threshold.

TABLE VIII
COMPARISON OF "EQUALIZED" NEF VALUES

Position	Test Phase	NEF Value
A	Initial and A	35.9
В	Initial	26.9
C	Initial	26.6
D	A	20.4
E	A	18.1
F	A	19.9

The equalized NEF value for position A is the mean value for the two test phases. Equalized NEF values for the remaining positions were computed by adjusting the mean NEF values for the position (as listed in Table VII) by the difference between the



COMPARISON OF EQUALIZED NEF VALUES FOR THE INITIAL PHASE AND PHASE A TESTS ٠ . FIGURE

mean NEP value observed at position A (over the same time period) and the equalized NEF value at position A.*

In Fig. 9, the NEF values are bracketed by a curved shaded band. In addition, near-horizontal bands intersect the curved band to indicate probable NEF values during level flight portions of the two approach procedures. The negative slope of near-horizontal bands reflects the gradual reduction in noise exposure expected to result from the reduction in number of observed overflights at increasing distances from the runway threshold.

From the presentation of NEF values, as described above, the difference in NEF values occurring at distances of approximately 80,000 ft from threshold or greater is slightly greater than 6 dB. This difference is in good agreement with the difference in mean noise levels, depicted in Fig. 8. Thus, both mean EPNL and NEF values, equalized to remove differences in volume of operations, show a consistent reduction of about 6 dB resulting from the increase in ILS intercept altitudes.

^{*} For example, the mean adjusted NEF value at position A for the two days at which measurements were made at position E is 37.2 (the "energy" average of 37.8 and 36.4). The difference between 37.2 and the equalized NEF value at position A, 35.9, is 1.3. Thus, the equalized NEF value at position E is 19.4-1.3, or 18.1.

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- 4. Federal Aviation Regulations, Part 36, "Noise Standards: Aircraft Type Certification".
- 5. "Supporting Information for the Adopted Noise Regulations for California Airports", Wyle Laboratories Poport No. WCR 70-3(R), January 1971.
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- 7. "Specification for General Purpose Sound Level Meter", United States of America Standards Institude, USAS S1.4, January 1961.

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- 8. "Frequency Weighting Network for Approximation of Perceived Noise Level for Aircraft Noise", Society of Automotive Engineers ARP 1080, July 1969.
- 9. "Definitions and Procedures for Computing the Perceived Noise Level of Aircraft Noise", Society of Automotive Engineers ARP 865A, August 1969.

APPENDIX

DATA ACQUISITION AND REDUCTION INSTRUMENTATION

This appendix describes the data acquisition equipment used in the field and the instrumentation used in the laboratory for data reduction. Individual paragraph references are keyed to pertinent sections of PAR Part 36.

A. Noise Measuring Equipment

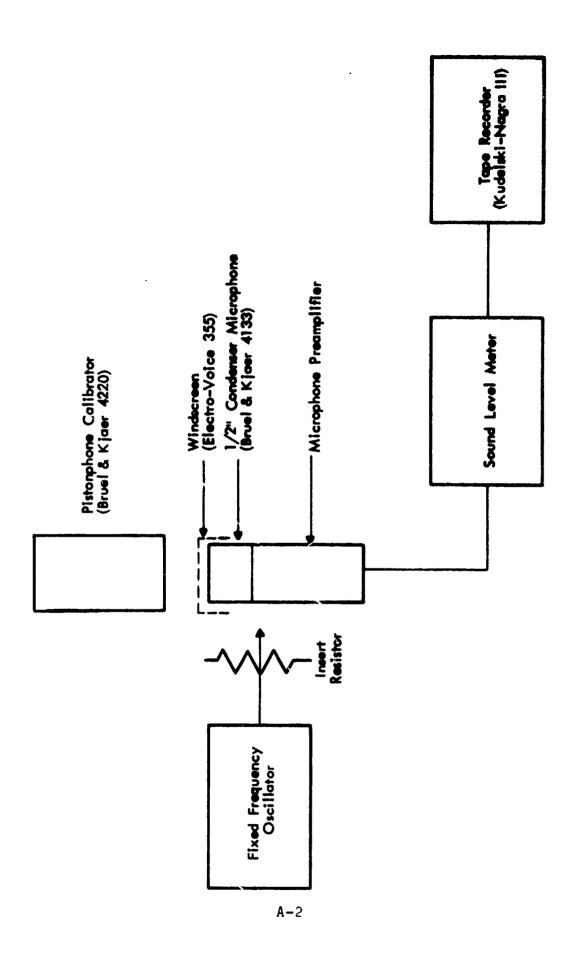
Each measurement station had self-contained recording capacity, with the instrumentation indicated in Fig. A-1. The system consists of a Bruel and Kjær Type 5144, 1/2-inch diameter, condenser microphone, a Bruel and Kjær Type 2619 preamplifier (or Hewlett-Packard 15108B Preamplifier), a Bruel and Kjær Type 2203 Precision Sound Level Meter, and a Kudelski Nagra III Tape Recorder. An Electro-Voice Model 355 Wind Screen was used over the microphone at all times.

A36.2(b)

The basic system response falls within the specifications of IEC Publication No. 179 "Precision Sound Level Meters". The response of the complete system was well within the tolerances specified in IEC Publication No. 179 as to sensitivity to a constant amplitude, sensibly plane progressive sinusoidal wave.

A36.2(c)(2)

Field calibrations of the system were performed before and after recording aircraft noise. The overall system response was verified by use of a 1,000 Hz sinewave oscillator driving an insert resistor at the input to the microphone preamplifier. Overall acoustic sensitivity of the system was obtained through recording the output signal of a Bruel and Kjaer Type



BLOCK DIAGRAM OF FIELD MEASUREMENT EQUIPMENT FIGURE A-1.

4220 Pistonphone Calibrator on the tape recorder through the system. Ambient noise levels and system electrical background noise were also recorded.

A36.2(e)(2),(3)

In addition to the basic meteorological data, obtained from the ESSA weather bureau at Metropolitan Airport, individual measurements of wind speed, temperature, and humidity were also made at each noise monitoring station. A Weksler 315-1 Sling Psychrometer and a Dwyer Windmeter were used to obtain these data.

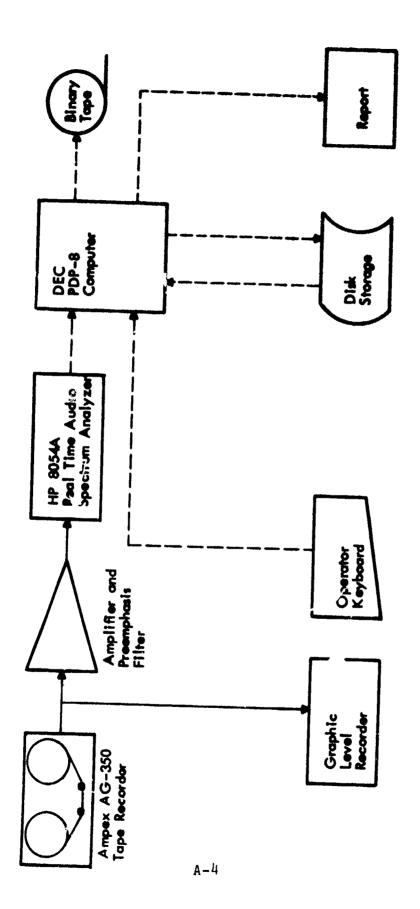
A36.3(b)(3)

B. Noise Analysis Equipment

All noise measurements were analyzed by a real time spectral analysis system. A block diagram of this system is shown in Fig. A-2. The primary elements consist of a Hewlett-Packard Model 8054A Real Time Audio Spectrum Analyzer, under control of a Digital Equipment Corporation Model PDP-8 Computer.

The tapes were played back on an Ampex AG-350 tape deck. For each of the three Kudelski Nagra III recorders there exists a correction spectrum which enables the computer to correct the signal, recorded on that Nagra and played back on the AG-350, to a flat response. In order to make maximum use of the available dynamic range a preemphasis filter was employed to attenuate the low frequencies. The insertion loss curve is presented in Fig. A-3. Along with the computer sampling, a graphic level record is made of the tape. This enables the operator to select starting and stopping points of the analysis and to determine where to select a sample of the background noise.

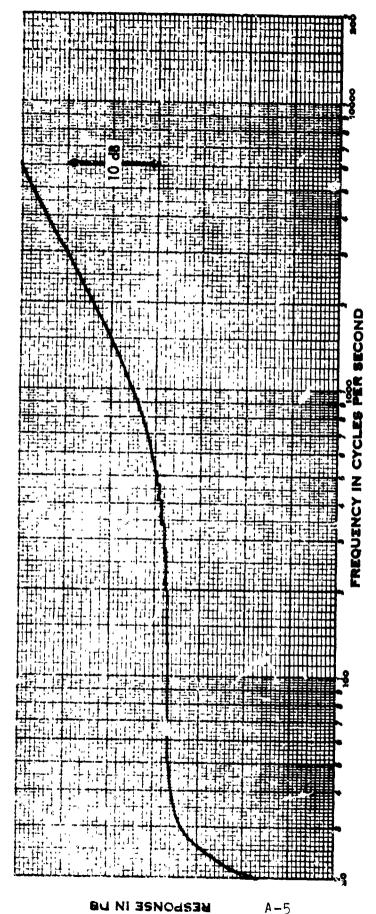
A36.2(d)



BLOCK DIAGRAM OF LABORATORY ANALYSIS EQUIPMENT FIGURE A-2.

1.3

· l



FILTER PREEMPHASIS CURVE OF INSERTION LOSS FIGURE A-3.

During the course of the analysis a sample is obtained every 0.5 seconds at the cutput of the 24 consecutive 1/3-octave bandwidth filters. (Center frequencies are from 50 Hz to 10 kHz.) The time sampling interval is derived from a 1-microsecond crystal clock and the accuracy of determining the 1/2-second intervals is within 5 microseconds. For each of the 0.5 second samples, approximately 30 milliseconds is required to read out the 24 1/3-octave bands, well within the 50 millisecond requirement. In a given frequency band the time for data transfer is 1 millisecond, well under the 5 milliseconds permissible.

A36.2(5)

The spectral analysis system exceeds all the requirements of IEC Publication No. 225, "Octave, dalf-octave, Third-octave Band Filters Intended for the Analysis of Sounds and Vibrations". The analysis system further meets the requirements on dynamic response, crest factor, linearity, dynamic range specified in Part 36. The resolution of the overall system is 0.1 dB. The overall accuracy of the system is ±0.1 dB in terms of output level with respect to input signal.

The values of several weighted noise levels are computed for each 1/2-second sample. Important spectral information and a summary of the weighted functions, their 10 dB down duration time and integrated values are printed by the computer, as shown in Fig. A-4.

C. Calibration Procedures

Microphones - Absolute sensitivity of the condenser microphones was determined through use of a General Radio Type 1559-B Microphone Reciprocity Calibrator. A36.2(c)

A74

		1/3 OCT	AVE BAND	CENTER	FREGU	ENCY			
56	63	80	100	125	160	200	250	315	400
MAXIMUM	VALUES	******							
67.0	66.9	64.3	70.5	71.9	71.8	69 - 1	12.3	69 . 11	71.0
69.9	69 . 6	60.6	67 • '	73.2	77.1	77.z	72.3	75.5	65.4
60 - 1	49 . 7	*****	*****						
AT PNLT	MAX								
****	****	****	****	66 • 6	68 • 1	63.6	66-5	67.9	66.8
67.4	67.2	67.8	67.8	73.0	77.1	71.4	71.7	75.5	65.8
66 - 1	49.5	****	*****						

NOISE LEVEL SUMMARY

MEASURE	TIME	MAX	1008 DUR	INTEGRAL

A-LEVEL	22.5	83.8	16.5	91.5
D-LEVEL	22.5	90.3	15.5	98.6
PNL	22.5	95.4	13.0	103.8
PNLT	22.5	97.4	15.0	105.7
TONE	18.3	2.7	(2000 HZ	BAND)

PNI.C = 96.9 EPNL = 95.7 SENEL = 91.5

A75

		1/3 OCT	AVE JAND	CENTER	FREOU	ENCY			
50	63	80	100	125	160	200	256	315	400
MAXIMUM	VALUES	****	****						•••••
61.6	65.7	****	68 • 2	78.9	69.7	68.9	67-6	67.2	66.6
65.4	63.9	63.7	63 .6	63.6	62.2	62.3	63. :	60.8	56.3
46.4	36.7	****	****						
AT PNLT	MAX								
****	****	****	68 • 🗗	69.2	68 • 8	30 . 5	67.6	64.4	66.3
64.8	63.9	52.9	63.6	63.2	61.9	\$1 . F	61.9	59 . 1	54.9
44.6	35.9	****	****						

NOISE LEVEL SUMMARY

MEASURE	TIME	MAX	1008 DUR	întegkal
		•••••		
A-LEVEL	19.5	73.1	22.5	54-0
D-LEVEL	25.Ø	79 - 1	22.0	89 • 8
PNL	19.5	85.1	20.5	75.6
PNL T	19.5	86.0	20.5	96.1
TONE	16.5	1.6	(3150 HZ	BAND)

PNLC = 86.6 EPNL = 86.1 SENEL = 84.0

FIGURE A-4. SAMPLE OF COMPUTER PRINTOUT

Sensitivity as a function of frequency was determined through the use of a Bruel and Kjaer Type 4142 Microphone Calibration Apparatus. This equipment consists of an electrostatic actuator and precision cavity. A General Radio Type 1304-B Beat Frequency Audio Generator is used to drive the input of the electrostatic actuator. The output of the microphone is recorded on a General Radio Type 1521-A Graphic Level Recorder.

The directivity pattern for the microphone is a function of the geometry of the microphone. Directivity patterns for a Bruel and Kjaer 4133 Microphone have been verified in our anechoic chamber.

The free field insertion loss introduced by the Electro-Voice Model 355 Windscreen has been determined by comparison of the outputs of two identical microphone systems, one with windscreen and one without, as exposed to an audio sweep frequency presented in an anechoic chamber. Over the frequency range from 45 to 11,200 Hz the insertion loss provided by this windscreen is zero to 4,000 Hz, 1 dB at 8,000 Hz, and 1.5 dB at 12,000 Hz.

Sound Level Meters - The Bruel and Kjaer Type 2203 Precision Sound Level Meter employed in the field measurement system provides both an amplifier and a precision attenuator between the microphone and the tape recorder. The frequency response of the sound level meter has been obtained by recording a sweep frequency over the range from 45 to 11,200 Hz and recording the output of the sound level meter on the level recorder as described under the microphone calibration above. All systems show the frequency response characteristics to be well within the tolerances specified by IEC Publication 179.

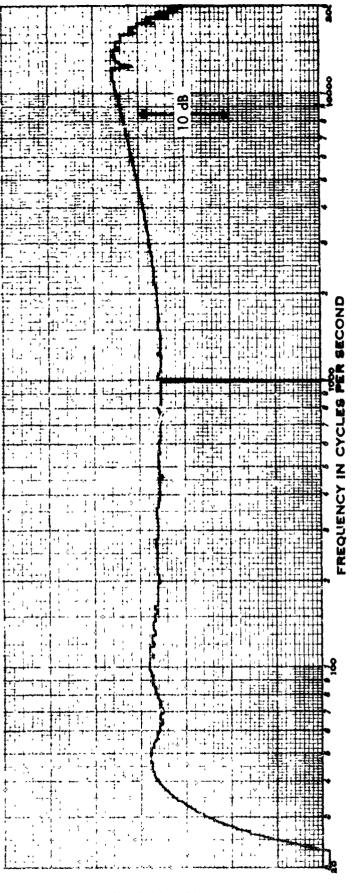
A separate evaluation of the accuracy of the attenuator in each sound level meter was obtained by applying a constant input voltage at the input of the sound level meter, while observing the attenuator output voltages for various settings with a digital voltmeter. In all cases the attenuator inaccuracies were found to be less than 0.1 decibels Ampex AG-350.

Tape Recorders - Each Kudelski-Nagra III tape recorder is individually evaluated in terms of its frequency response and dynamic range capability. Each of the tape recorders if modified in such a way that no pain adjustment on the recorder is possible in the field. Input level adjustments are all obtained through the use of the attenuator in the Brue' and Kjaer sound level meter. Therefore, the changes in attenuator settings for the overall system are those determined above for the Bruel and Kjaer sound level meter, namely, within 0.1 decibels per step.

The overall dynamic range of each of the tape recorders has also been determined. Nominal signal-to-noise ratio capability for less than 3% overall distortion is 52 decibels for the tape recorders. This, of course, indicates a dynamic range in excess of 60 dB in any given frequency band.

Overall Recording System Response - The complete recording and analysis system is calibrated by a sinusoidal signal which is swept over the entire frequency range of the system. The signal is introduced by use of an insert resistor between the condenser microphone and the preamplifier. Thus a complete sine wave calibration is available from 45 to 11,200 Hz. A response curve of such a sweep played back on the Ampex AG-350 used for data reduction is shown in Fig. A-5.

A36.2(c)(3)



Seurch General Radio Type 1304-B Beat Frequency Audio Generator (S/Recorded: Through Bruel & Kjaer Type 2203 Sound Level Meter (S/N 1129 Kudelski Nagra III (S/N 8340) 15 lps, CCIR, Ampex 641 Tapin Piaytrck: Ampex AG-350 (S/N £453231), Equalization +5 dB @ 10 kHz General Radio Type 1521-A Graphic Level Recorder (S/N 288)

URE A-5. RECORD PLAYBACK CHARACTERISTIC: STATION B / AMPEX AG-350

BO NEESNOUSEN

Analyzer - The characteristics of the analysis system are primarily determined by the Hewlett-Packard 8054A Real Time Spectrum Analyzer. This analyzer has a set of 24 consecutive 1/3-octave filters with geometric mean frequencies covering the range from 50 Hz to 10 kilohertz. The filter characteristics are well within the specifications provided in IEC Publication No. 225.

The detection of filter output is performed by a quasi-RMS detector. We have evaluated the performance of this detector by recording successive bursts of sine wave signals of varying duration where the frequency of the sine wave is that of the geometric mean frequency of each filter. By these tests we have verified that, up to crest factors of 5, the output of the analyzer is within less than 1 dB of a true root-mean-square value for the signal in each of the frequency bands. Examining the response to a sinusoidal pulse of 0.5 second ration at the geometric mean frequency of each 1/3-octave band applied to the input, we find that the maximum output signal is 4±0.1 decibels less than the value attained from a steady state signal of the same frequency and amplitude, verifying the signal averaging time of the analyzer.

A36.2(a)(4)

The maximum output value of the analyzer is less than 0.5 dB different from the final steady state value obtained when a steady sinusoidal signal at the geometric mean frequency of each 1/3-octave frequency band is suddenly applied to the analyzer input and held constant.

The amplitude resolution of the analyzer is 0.1 dP.

Repeated analysis of the same recorded random signal provides an output indication from the analyzer which is repeatable within 0.1 dP at all frequency bands.

A36.2(d)(6)

D. Meteorological Equipment

The psychrometers used for determining temperature and humidity permit resolution to within 0.5 degrees F. This permits calculating relative humidity to within 3% for the temperature range observed.

The Dwyer windmeters permit resolution of wind speed to within 1/4 mph. in the range from 2 to 10 mph., and within 1 mph. in the range from 6 to 60 mph.

A36.3(b)(2)